

**VISTA DE SANDIA SUBDIVISION
SANTA FE COUNTY, NEW MEXICO
HYDROGEOLOGIC REVIEW**

Prepared For:

Vista De Sandia Corp.
1533 St. Francis Drive, Suite C
Santa Fe, N.M. 87501

Prepared By:

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Santa Fe, New Mexico

August, 1994



HYDROGEOLOGIC REVIEW
SECTIONS 21 AND 22, T16N, R8E
SANTA FE COUNTY, NEW MEXICO
by Jack P. Frost, Hydrogeologist

Prepared for Mr. Louis Gonzales, the Brokerage Realty

INTRODUCTION

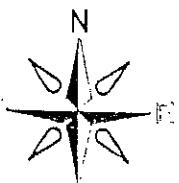
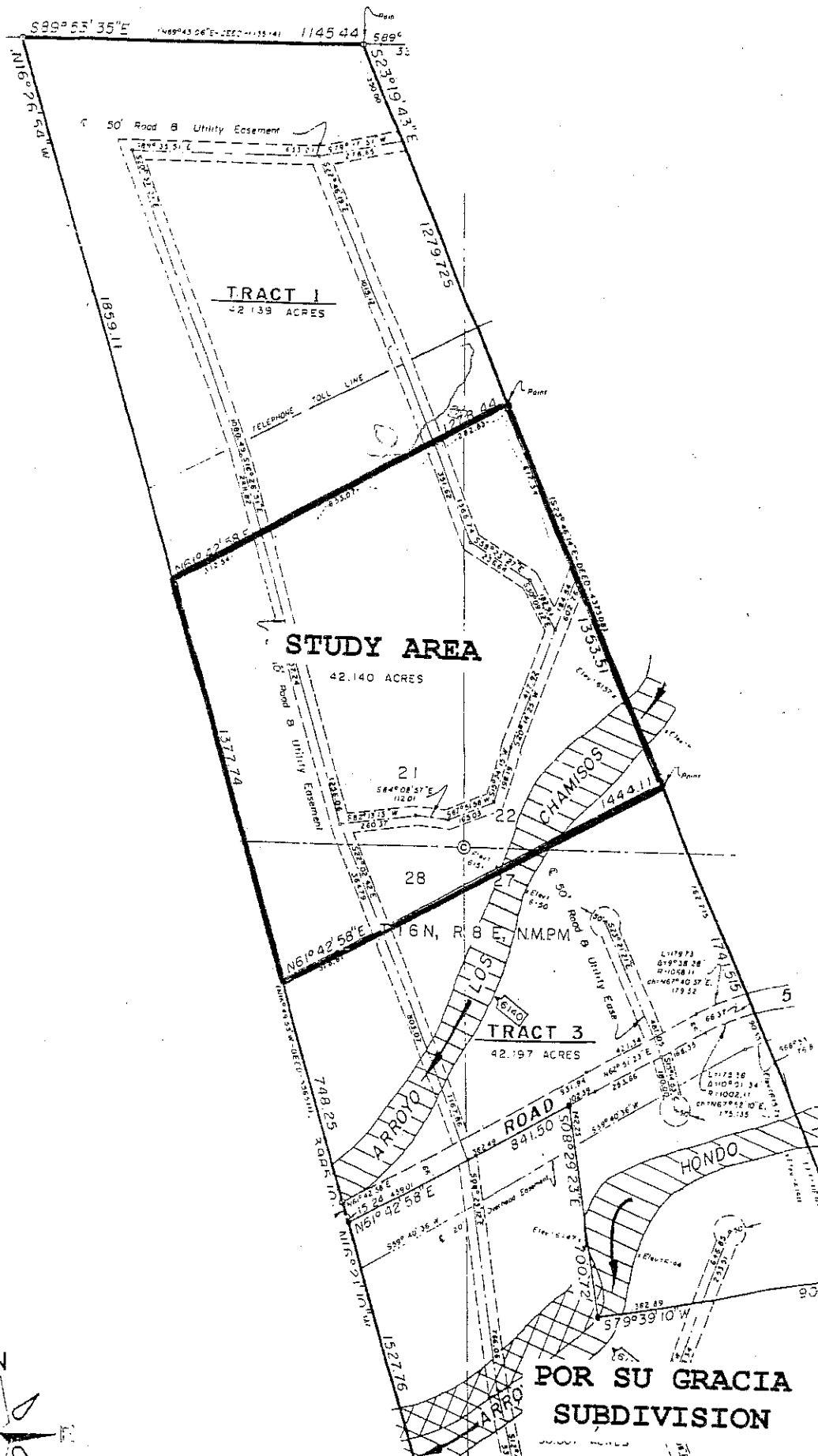
Following are findings of a review of the ground water resource in the vicinity of a 42 acre tract near La Cienega and the Santa Fe airport (Figure 1). The area occupies portions of the southeast quarter of section 21, and the southwest quarter of section 22, T16N, R8E, Santa Fe County, NM. This study supplements the Por Su Gracia Water Resource Study dated June, 1994 (attached) and reviews additional wells north of Arroyo Chamiso.

To minimize impacts on the shallow water table, and to minimize septic tank contamination, a suggested well design follows.

AQUIFER DESCRIPTION

For the greater Santa Fe area, the study area is blessed with an above average water resource. Groundwater occurs in the Ancha and Tesuque formations, occupying part of the greater Santa Fe basin. The aquifer is composed of sand, gravel, silt and clay. The aquifer is moderately to highly stratified, and ground water flow is primarily horizontal, to the south-southwest.

The Ancha rests on a eroded unconformity on top of the Tesuque formation. It has been differentiated from the underlying Tesuque in that it is more coarse grained and less cemented and consolidated. The Tesuque formation often contains more clay and silt beds. The two aquifer zones are difficult to distinguish in most drillers logs.



85
FIGURE 1

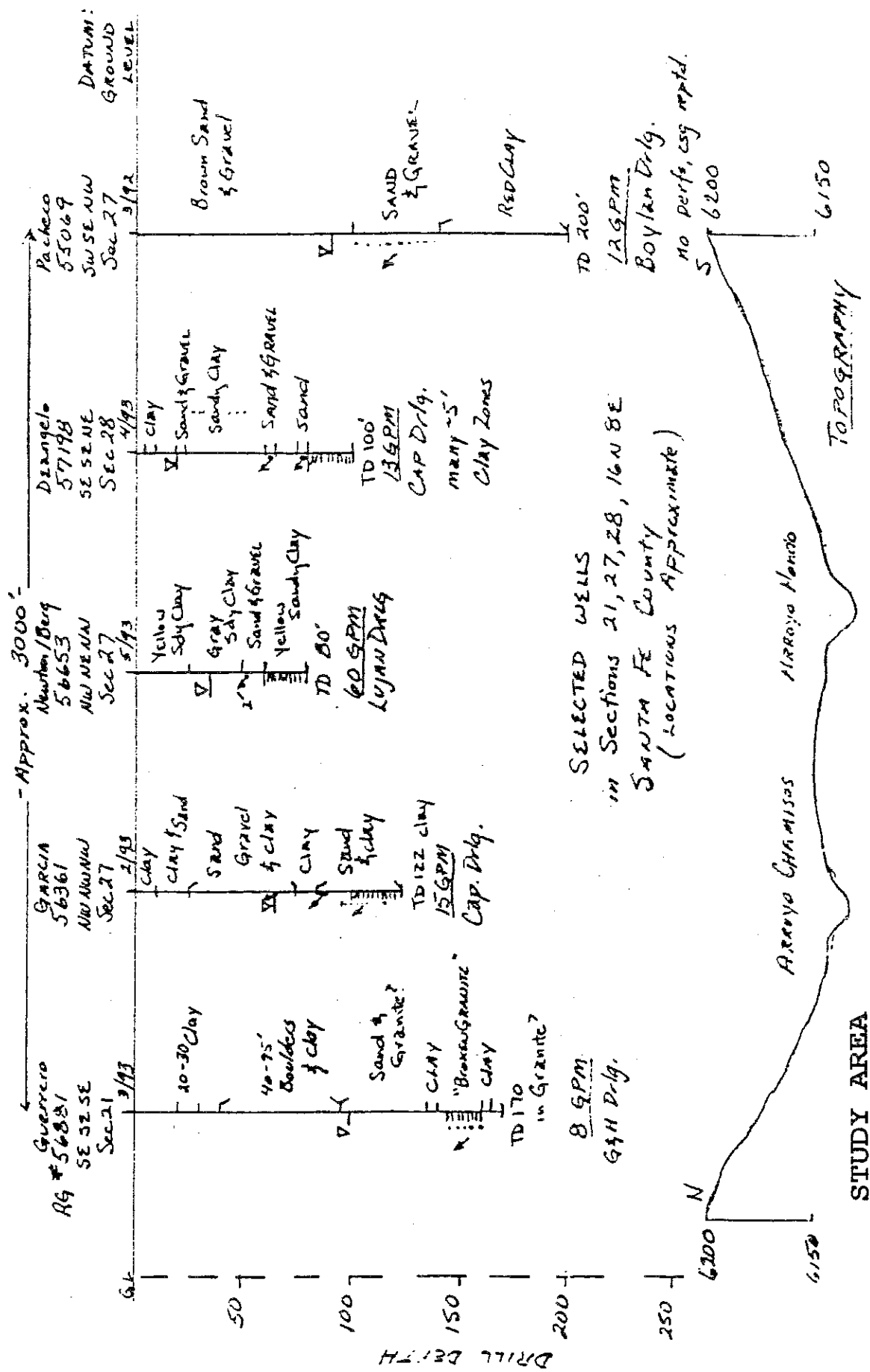


Figure 2 SCHEMATIC CROSS SECTION

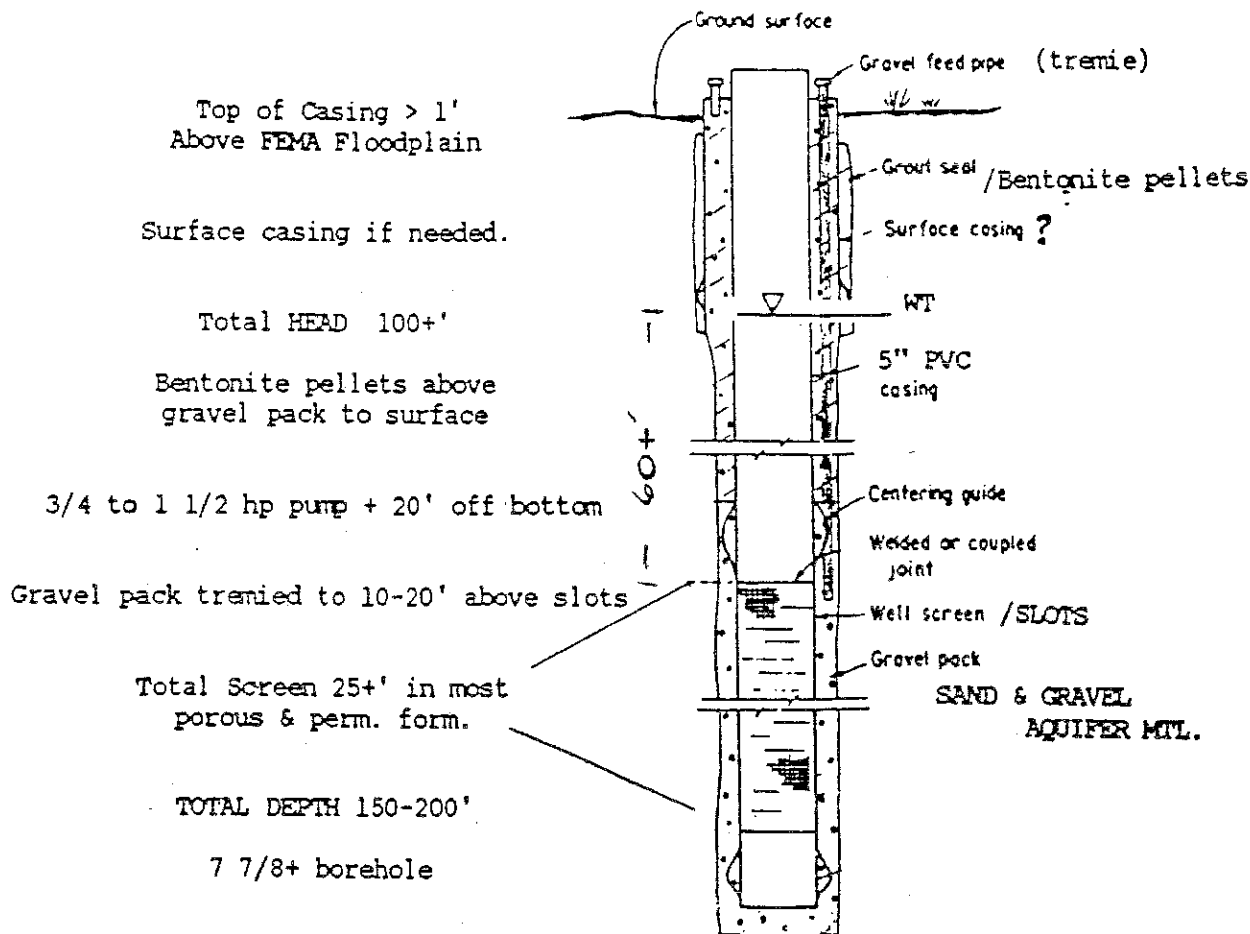
GROUND WATER DEVELOPMENT

The average total depth of over 25 nearby domestic wells is about 140 feet (Table 1). The wells encountered water at about 60 feet (varying with topography) and have an average yield of 35 gallons per minute. The yield is dependent on the net thickness of sand and gravel encountered. Figure 2 illustrates wells in the area.

There are a number of irrigation and commercial water rights in the area, including the race track. Such demands on the aquifer are much greater than a domestic well. The water table may fluctuate seasonally or due to high commercial demand.

One well drilled nearby reported drilling granite. The Guerrero well, RG-56881, Figure 2 and attached, reported drilling boulders, sand and granite, and clay and granite. Several other wells reported coarse gravels and boulders. This well is difficult to explain, other than the fact that the driller has limited experience in this area and may have misinterpreted granite boulders and coarse outwash known to be present in buried stream channels in the section. The well was completed for 8 gpm.

According to a report by Fleming, 1994, the Ancha has a maximum thickness of about 66 feet of groundwater saturation in this area. Most of the domestic wells reviewed in the attached table are completed, at least in part, in the Ancha. Several wells are perforated near the water table, which makes them vulnerable to any contaminants that might seep down, such as septic tank effluent. The race track well is reported to include perforations in the Ancha.



SINGLE STRING CONSTRUCTION

FIGURE 11-1.—Gravel packed, rotary drilled well for single string construction. 103-D-1488.

SUGGESTED PROTOTYPE WELL DESIGN
TO PRODUCE FROM THE TESUQUE FORMATION
AND ISOLATE THE ANCHA FORMATION

Prepared by: Jack P. Frost
Hydrogeologist
505-466-6435

Modified from the Ground Water Manual

The Ancha formation has been interpreted as the principal source of spring flows at La Cienega and Guicu Creeks. It has been recently suggested that the Ancha should be cased off from production in new domestic wells. If designed and constructed properly, a domestic well can isolate the Ancha and produce exclusively from the Tesuque.

A prominent spring in the approximate groundwater flowpath of this area is at Sunrise Springs resort. In a study for the resort prepared by AGW Consultants, 1986, they interpreted that the Ancha is either thin or above the water table in the vicinity of the spring. The AGW report agreed with Spiegel and Baldwin, 1963, that the spring flows are associated with the Ancha and Tesuque aquifer adjoining much less permeable volcanic rocks where they subcrop in the vicinity of La Cienega. Groundwater flow is deflected upward at this contact. Based on published sources, this boundary lies about one mile southwest of the study area.

SUGGESTED WELL DESIGN

Whatever the actual subsurface conditions may be, the most effective way to minimize impacts and protect water quality is to isolate the Ancha and complete the well in deeper sand and gravel formations. A suggested well design is illustrated in Figure 3. The most important components in this design are 1, perforations greater than 60 feet below the water table, and 2, a bentonite pellet backfill in the annular space above the gravel pack/ stabilizer opposite the slots or perforations. Total depth of this design will be about 200 feet.

The Tesuque formation is expected to possess a Specific Capacity of approximately 1 gallon per minute per foot. Thus a domestic well with more than 25 feet of slots in porous sand and gravels should be able to yield up to 20 gpm.

SUMMARY AND RECOMMENDATIONS

The area of the proposed subdivision is underlain by the combined Ancha - Tesuque formation aquifer. Groundwater production is from sand and gravel beds interstratified with silts and clays. An adequate resource exists for domestic purposes.

In order to protect the shallow water table and to isolate production from potential contamination, a well design (Figure 3) is recommended. Wells should be slotted or perforated in sand and gravel at least 60 feet below the water table, gravel packed, and the overlying annular space should be backfilled with bentonite pellets.

Water conservation measures and covenants should be adopted to conserve the resource. To conserve costs, shared wells should be considered. Wells with yields of 20 to 25 gpm could be shared by up to four houses.

Because of the presence of permeable soils and a shallow water table, careful consideration should be given to the location and construction of septic fields and wells.

Well Number	Owner Name	Location	Date	Total Depth	Depth to Water	Yield (GPM)	Water Column	Depth to PWBF	Depth to Base of Low Zone	Estimated Elevation	Water Table (WT)	Principal Water Bearing Formation	Drilling Contractor
✓ 56348	Casb	SE NE NE 28	Nov-92	165	40	20	125		165			Red Gravel and Blue Clay	Gardia's
✓ 56361	Garcia	NW NW NW 27	Feb-93	122	65	15	57	96	115			Snd & Gvl 65-75, Snd & Gvl 85-90, Sand 96-115	Nuanes-Cap Boylan
✓ 56069	Pacheco	SW SE NW 27	Mar-82	200	90	12	110	100	140			Sand and Gravel	Boylan
✓ 56650	Newton	NW NE NW 27	May-94	80	35	60	45	50	52			Yellow Sand and Gravel	Lujan
✓ 57198	Deanpelo	SE SE SE 28	Apr-93	100	19	13	81	75	80			Snd & Gvl 19-22, Snd & Gvl 60-85, Sand 75-80	Nuanes-Cap
✓ 58393	Gallegos	SE SE SW 22	Oct-93	108	64	20	44	64	95			Sand and Gravel	Nuanes-Cap
✓ 58245	Montoya	SE SE SW 22	Oct-93	117	69	20	48	69	117			Sand and Gravel	Nuanes-Cap
✓ 56881	Guerra	SE SE SE 21	Mar-93	170	100	8	70	145	180			Pk Bkn Granite	G&H
✓ 21468		SE SW SW 22	Aug-72	72	28		44	59	69			Bm, Red Sand	Crocker Lujan
✓ 56653		NW NE NW 27	May-83	80	35	60	45	50	52			Yel. Sand & Gravel	Nuanes-Cap
✓ 56361		NW NW NW 27	Feb-93	122	65	15	57					Sand and Gravel	Boylan
✓ 56069		SW SE NW 27	Mar-92	200	90	12	110					Sand and Gravel (poor)	Garcia
✓ 56348		SE NE NE 28	Nov-92	165	40	20	125					Red Grav., Blue Clay and Gravel	Nuanes-Cap
✓ 56393	Gallegos	SE SE NE 28	Apr-83	100	19	13	81	64	95			Sand, Sand and Gravel	Nuanes-Cap
✓ 58245	Montoya	SE SE NW 22	Oct-93	108	64	20	44		44			Sand and Gravel	Nuanes-Cap
✓ 58411	Gallegos	SW SE 22	Oct-93	117	69	250	48					Gravel	Nuanes-Cap
✓ 55680	Holmes	NE NW SW 27	Oct-93	105	61	20	44					Layers of Sand and Gravel	Nuanes-Cap
✓ 55355	Romero	NW NE SW 27	Sep-92	200	80	20	120	25	75			Red and White Clay and rock	Boylan
✓ 55154	Madrid	NW NE SE 28	May-92	200	100	10	100					Sand and Gravel	Nuanes-Cap
✓ 41553	Gallegos	SW SE SW 22	Apr-82	90	33	20	57					Sand, Sand and Gravel	Boyal
✓ 41775	Cook	SE SE SW 22	May-84	100	42	15	58					Brown Sand and Gravel	Boylan
✓ 42782	Pino	SE SE SW 22	Nov-84	373	125	150	249	120	370			Gray Silt	Boylan
✓ 56838	McNeil	NW SE NW 28	Nov-84	90	20	20	70	20	80			Sand and Gravel	Nuanes-Cap
✓ 56178		SW NE NE 28	Apr-93	160	99	20	61	53				Wash and Boulders	Thompson
✓ 57760		NE NE SE 28	Sep-92	195	75	7	120	120				Bm/Red Sand	Crocker
✓ 21468	Quinlana	SE SW SW 22	Aug-72	72	28		44	31	69				
Averages:				139	60	35	76	67	108				

denotes wells adjoining the study area

TABLE 1

STATE ENGINEER OFFICE

WELL RECORD

Section 1. GENERAL INFORMATION

(A) Owner of well G. S. de Guzman Gerardo Guerrero Owner's Well No. '93 APR 28 AM 10
 Street or Post Office Address 1817 Mann St
 City and State Santa Fe N.M. 87501

Well was drilled under Permit No. RG-56881 and is located in the:

a. SE $\frac{1}{4}$ SE $\frac{1}{4}$ SE $\frac{1}{4}$ of Section 21 Township 16N Range 8E N.M.P.M.

b. Tract No. _____ of Map No. _____ of the _____

c. Lot No. _____ of Block No. _____ of the _____
 Subdivision, recorded in SANTA FE County.

d. X= _____ feet, Y= _____ feet, N.M. Coordinate System _____ Zone in
 the _____ Grant.

(B) Drilling Contractor G&H Drilling *pretty acc.* License No. WD 815

Address 5730 Greer LP Sw Albuq. 87105

Drilling Began 3/5/93 Completed 3/9/93 Type tools Rotary Size of hole 7 7/8 in.

Elevation of land surface or _____ at well is _____ ft. Total depth of well 170 ft.

Completed well is ☒ shallow ☐ artesian. Depth to water upon completion of well 100 ft.

Section 2. PRINCIPAL WATER-BEARING STRATA

Depth in Feet		Thickness in Feet	Description of Water-Bearing Formation	Estimated Yield (gallons per minute)
From	To			
145	160		Pink broken granite	about 8

Section 3. RECORD OF CASING

Diameter (inches)	Pounds per foot	Threads per in.	Depth in Feet		Length (feet)	Type of Shoe	Perforations	
			Top	Bottom			From	To
5	PVC		1 $\frac{1}{2}$	170	171 $\frac{1}{2}$	Open	150	170

Section 4. RECORD OF MUDDING AND CEMENTING

Depth in Feet		Hole Diameter	Sacks of Mud	Cubic Feet of Cement	Method of Placement
From	To				

93 APR 20 P 1:2
 DISTRICT 1
 ALBUQUERQUE, N.M.

92

[illegible]

WELL RECORD

INSTRUCTIONS: This form should be executed in triplicate, preferably typewritten, and submitted to the nearest district office of the State Engineer. All sections, except Section 5, shall be answered as completely and accurately as possible when any well is drilled, repaired or deepened. When this form is used as a plugging record, only Section 1A and Section 5 need be completed.

Section 1

(A) Owner of well GARY GOINTANA
 Street and Number RT 4 BOX 94
 City SANTA FE State N.M.
 Well was drilled under Permit No. RG 21468 and is located in the
SE 1/4 SW 1/4 of Section 22 Twp. 16-N Rge. 8-E
 (B) Drilling Contractor CROCKER, INC. License No. WD 214
 Street and Number RT 4 BOX 94
 City SANTA FE State N.M.
 Drilling was commenced AUG 29 19 72
 Drilling was completed AUG 29 19 72

(Plot of 640 acres)

Elevation at top of casing in feet above sea level _____ Total depth of well 72'
 State whether well is shallow or artesian SHALLOW Depth to water upon completion 28'

Section 2

PRINCIPAL WATER-BEARING STRATA

No.	Depth in Feet		Thickness in Feet	Description of Water-Bearing Formation
	From	To		
1	31	51	20	BROWN SAND
2	59	69	10	BROWN-RED SAND
3				
4				
5				

STATE ENGINEER OFFICE
 SANTA FE, N.M.
 1972 SEP 22 AM 11 25

Section 3

RECORD OF CASING

Dia. in.	Pounds ft.	Threads in.	Depth		Feet	Type Shoe	Perforations	
			Top	Bottom			From	To
4 1/2	70	—	0	72	72	—	50	68
							28	33

Section 4

RECORD OF MUDDING AND CEMENTING

Depth in Feet		Diameter Hole in in.	Tons Clay	No. Sacks of Cement	Methods Used
From	To				

STATE ENGINEER OFFICE
 SANTA FE, N.M.
 1972 SEP 25 AM 11 18

Section 5

PLUGGING RECORD

Name of Plugging Contractor _____ License No. _____
 Street and Number _____ City _____ State _____
 Tons of Clay used _____ Tons of Roughage used _____ Type of roughage _____
 Plugging method used _____ Date Plugged _____ 19 _____
 Plugging approved by: _____

Cement Plugs were placed as follows:

No.	Depth of Plug		No. of Sacks Used
	From	To	

FOR USE OF STATE ENGINEER ONLY

Date Received SEP 22 1972File No. RG-21468 Use dam Location No. 16.8.22.334

Section 8

LOG OF WELL

[illegible]

The undersigned hereby certifies that, to the best of his knowledge and belief, the foregoing is a true and correct record of the above described well.

CHS 200-151 1-2
200-151 1-2
Edward Elcock
Well Driller

(B) DURING THE PERIOD OF THE INVESTIGATION, THE FOLLOWING INFORMATION WAS OBTAINED FROM THE RECORDS OF THE BUREAU OF THE DISTRICT ATTORNEY, NEW YORK CITY:

ACCEPTED

STATE ENGINEER OFFICE

WELL RECORD

Section 1. GENERAL INFORMATION

(A) Owner of well Helen P. Newton / Terry Berg Owner's Well No. _____
 Street or Post Office Address Rt. 14, Box 200
 City and State Santa Fe, NM 87501

'93 JUN 7 AM 10 26

STATE ENGINEER OFFICE
 SANTA FE NEW MEXICO

Well was drilled under Permit No. RG-56653 and is located in the:

a. 1/4 NW 1/4 NE 1/4 NW 1/4 of Section 27 Township 16N Range 8E N.M.P.M.

b. Tract No. _____ of Map No. _____ of the _____

c. Lot No. _____ of Block No. _____ of the _____
 Subdivision, recorded in Santa Fe County.

d. X= _____ feet, Y= _____ feet, N.M. Coordinate System _____ Zone in
 the _____ Grant.

(B) Drilling Contractor Lujan Drilling License No. WD-547

Address Rt. 3, Box 95-78, Santa Fe, NM 87505

Drilling Began 5-14-93 Completed 5-14-93 Type tools Rotary Size of hole 9 in.

Elevation of land surface or _____ at well is _____ ft. Total depth of well 80 ft.

Completed well is ☒ shallow ☐ artesian. Depth to water upon completion of well 35

Section 2. PRINCIPAL WATER-BEARING STRATA

Depth in Feet		Thickness in Feet	Description of Water-Bearing Formation	Estimated Yield (gallons per minute)
From	To			
50	52	2	Yellow Sand & Gravel	60 ?

Section 3. RECORD OF CASING

Diameter (inches)	Pounds per foot	Threads per in.	Depth in Feet		Length (feet)	Type of Shoe	Perforations	
			Top	Bottom			From	To
6 5/8			0	80			60	80

Section 4. RECORD OF MUDDING AND CEMENTING

Depth in Feet		Hole Diameter	Sacks of Mud	Cubic Feet of Cement	Method of Placement
From	To				

'93 JUN 25 AM 9
 STATE ENGINEER OFFICE
 SANTA FE NEW MEXICO

96

[illegible]

WATER RESOURCE STUDY AND WELL DESIGN
FOR SU GRACIA SUBDIVISION
SECTIONS 27 AND 28, T16N, R8E
SANTA FE COUNTY, NEW MEXICO

Prepared by: Jack P. Frost
Hydrogeologist
505-466-6435
January, 1994
Revised June, 1994

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PRE-DRILL REVIEW
POR SU GRACIA SUBDIVISION
WATER RESOURCE STUDY AND WELL DESIGN
SECTIONS 27 AND 28, T16N, R8E, SANTA FE COUNTY, N.M.

Prepared by: Jack P. Frost
Hydrogeologist
June, 1994

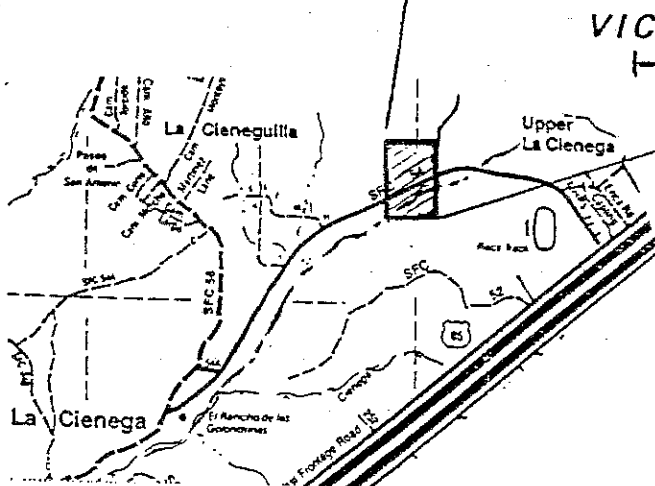
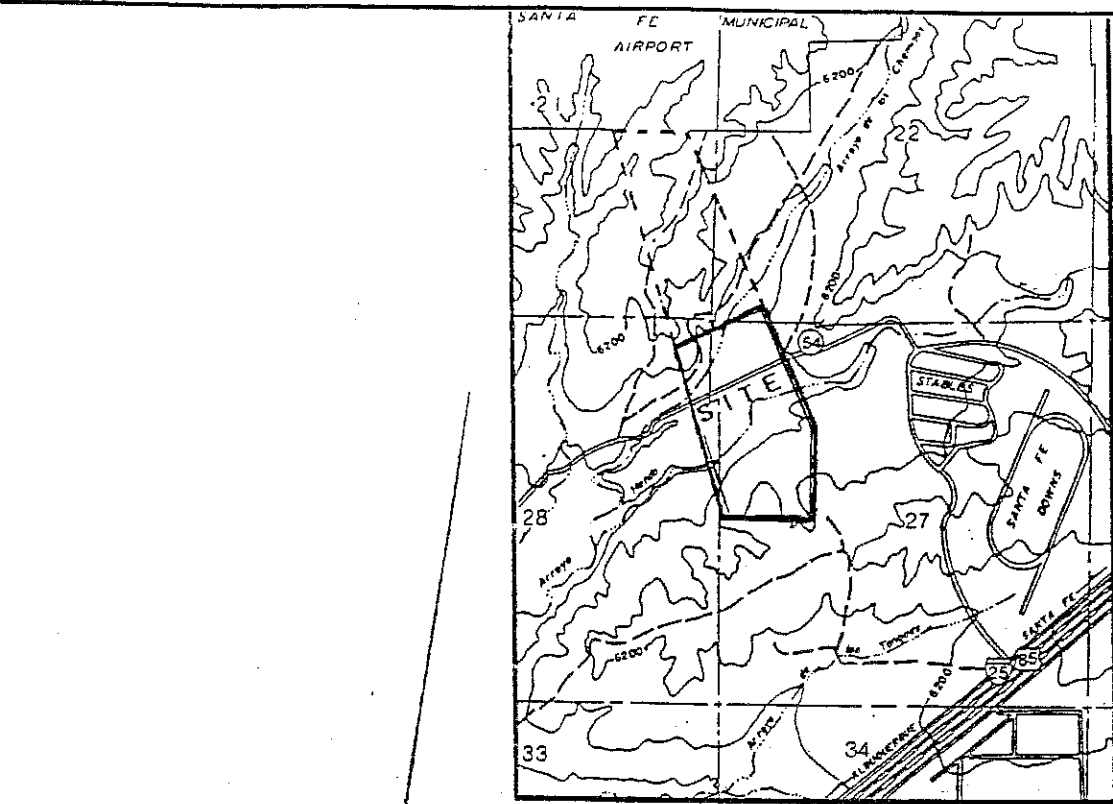
INTRODUCTION

This report reviews the hydrogeology in the vicinity of two adjoining forty acre tracts near La Cienega, Santa Fe County. Also included is a plan for a typical well design and distribution of shared wells. The owners propose to subdivide the parcels into approximately 2 1/2 acre tracts.

The premise of this study is that a shared well system, coupled with thoughtful well design and construction, will be economical and will minimize the impact on the shallow aquifer. Such a system will ensure a safe water supply for the future.

This study shares several features of the County Code - prescribed Hydrogeologic Report. The owners are not asking for increased lot density. It is their intent to adopt the 2 1/2 acre density allowed by the County Code in this area when dwellings are restricted to 0.25 acre feet per year of water, including water conservation measures.

The study area lies in the County's Extra - Territorial Zone, in the Basin Hydrologic zone. It flanks County Road 54 approximately 1 1/4 miles from the intersection with Racetrack Road. It lies west of the Santa Fe Downs race track in the valley of the confluence of Arroyos Chamiso and Hondo (Figure 1).



LOCATION OF THE POR SU GRACIA
AND BROWN TRACTS, SANTA FE COUNTY

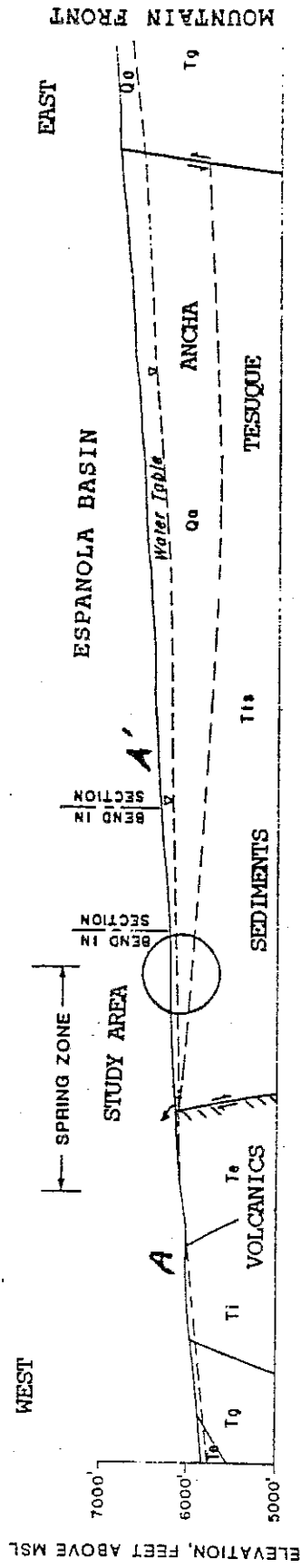
SCOPE

The scope of this project is a departure from common practices in the area. Typically individual landowners have drilled single - dwelling wells with little consideration of impact or contamination potential. From the review of well logs it appears that drillers' completion practices are highly varied.

Approximately 18 wells within a one - half mile radius were reviewed in this study. Over 90 wells and/or permits are on file at the State Engineer's Office within a one mile radius of the subject tract. From the well logs a cross section was constructed (Appendix 2) and the subsurface hydrogeologic conditions were interpreted. The well logs have also been helpful in designing a prototype well whose construction should protect the shallow Ancha Formation aquifer as well as minimize contaminant susceptibility from septic tank and other surface sources.

Several regional studies serve as important references for this report. They include Spiegel and Baldwin, 1963; and Fleming, 1994. Locally, several studies have been prepared to evaluate development at the Racetrack (Spiegel, 1975), and at Sunrise Springs Resort (AGW Consultants, 1976).

In order to optimize the number and distribution of shared wells on the property several computer models have been constructed to simulate drawdown and potential interference in the well field.



Q_a, Ancha Formation; T₀, Espinazo Volcanics; T_{1s}, Tesuque Formation; T₂, Gallateo Formation

SCHEMATIC HYDROGEOLOGIC CROSS SECTION

AFTER SPEIGEL

HYDROGEOLOGIC SETTING

The hydrogeologic setting of the study area is depicted in Figures 2 and 3. They are modified from the AGW Consultants' study at Sunrise Springs Resort.

The study area lies on the west flank of the Espanola Basin. The older Tesuque and Ancha Formations, and recent basin-fill sediments terminate against a fault about a mile west of the study area (Spiegel, 75). Relatively impermeable volcanic rocks adjoin the fault zone on the west, creating a groundwater flow boundary. Ground water flows westward from the mountains, and the water table "piles up", in effect, against the volcanic rocks and discharges through springs, streambeds and phreatophytes in the vicinity (Figure 3).

The subject tracts occupy the floodplain and flanking hillsides of Arroyos Chamisa and Hondo. The arroyos are underlain by alluvial sand and gravel, silt and clay derived from the mountains to the east. These deposits represent recent and Quaternary age outwash overlying and cut into the Tertiary Tesuque Formation.

The Tesuque Formation is composed of similar sediments which are more consolidated and cemented. Buried channels of coarse sediment probably occur within the section and influence ground water flow. The Ancha Formation, which unconformably overlies the Tesuque outside the Arroyo, is probably thin or may be absent beneath the valley floor (Spiegel 1963, Fleming 1993). Actual boundaries between these units are not distinguishable in most driller's logs.

Ground water occurs as an unconfined aquifer at depths of 30 to 60 feet in most of this area. Springs and stream bed seeps represent areas where the water table approaches ground level, often associated with geologic contacts or faults.

Local domestic wells are above average for Santa Fe County in terms of production rate, depth to water, and water quality. Domestic wells are partially penetrating, and range from 72 to over 370 feet in the area. The saturated thickness of combined Ancha - Tesuque sediments is greater than 1000 feet, as revealed by exploratory drilling (AGW Consultants, 1976).

Springs in the Area

Most of the springs and acequias in the area occur along the valley walls of arroyos that drain towards La Cienega, west-southwest of the study area. Based on Spiegel's and Fleming's regional maps, the study area is not in the flow path of groundwater moving towards these springs (Figure 2). In addition, the water table in the study area lies deeper than the discharge elevation of spring lines in Cienega and Guicu Creeks, one to three miles southwest.

Complicating the distribution of the springs is the faulting and degree of stratification in the sediments of the area. For example, at Sunrise Springs, ample groundwater flow (est. 18 gpm) occurs in sand, gravel and clay horizons from depths of 29 to 50 feet, where 15 feet of clay was encountered. The principal water bearing strata was reported as a 5' zone within 16' of "red clay and gravel". The "Sunrise Springs" could be perched flow horizon on the valley wall, where the water table reaches the surface. Spiegel also implicated igneous intrusions or the regional fault to explain these spring locations.

Aquifer Properties

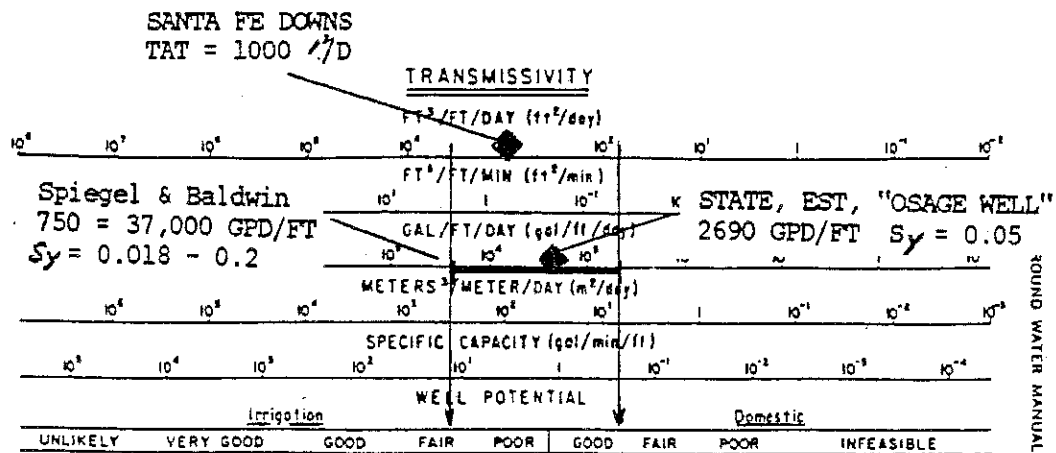
The sedimentary section appears to be moderately stratified, with interbedded sand and gravel, silt and clay (Appendix 1 and 2). Although moderately transmissive, the aquifer is heterogeneous and anisotropic. In such situations the downstream horizontal hydraulic conductivity is typically much higher than the lateral and vertical hydraulic conductivity (Walton, 1987). A ratio of horizontal to vertical hydraulic conductivity of 10 was used in models presented here.

The average reported hydrologic coefficients of the local formations were reviewed in the Sunrise Springs report. Based on a pump test and other data, that study concluded that an average Transmissivity of 10,000 gpd/ft and a Specific Yield of 0.10 is appropriate and conservative for the combined Ancha - Tesuque formations locally. A Specific Capacity of 1 gal per minute per foot of permeable formation is reasonable in this area. Figure 4 puts these values in perspective.

Using an average water table slope of 0.4 percent, average porosity of 5 percent, and an average hydraulic conductivity of 25 ft/d (31 ft/d was measured in the thin section at Sunrise Springs), the average linear velocity of flow is approximately 1.2 feet per day. Neglecting fracturing, vertical flow velocities are expected to be at least one tenth the rate of horizontal flow.

Recharge and Contamination Susceptibility

The arroyos flow within their channels seasonally. In this area the stream banks are incised and well defined. Small, seasonal stream flows represent groundwater discharge. Regional ground water through - flow is much larger than vertical recharge due to precipitation, although streambed recharge could be significant during flood events. The arroyos and buried channels are potentially significant conduits of groundwater flow from the mountains (Fleming, 94).



NOTES: Transmissivity (T) = KM where
K = Permeability
M = Saturated thickness of the aquifer
Specific capacity values based on pumping period of approximately
8-hours but are otherwise generalized.

FIGURE 2-4.—Comparison of transmissivity, specific capacity, and well potential. 103-D-1406.

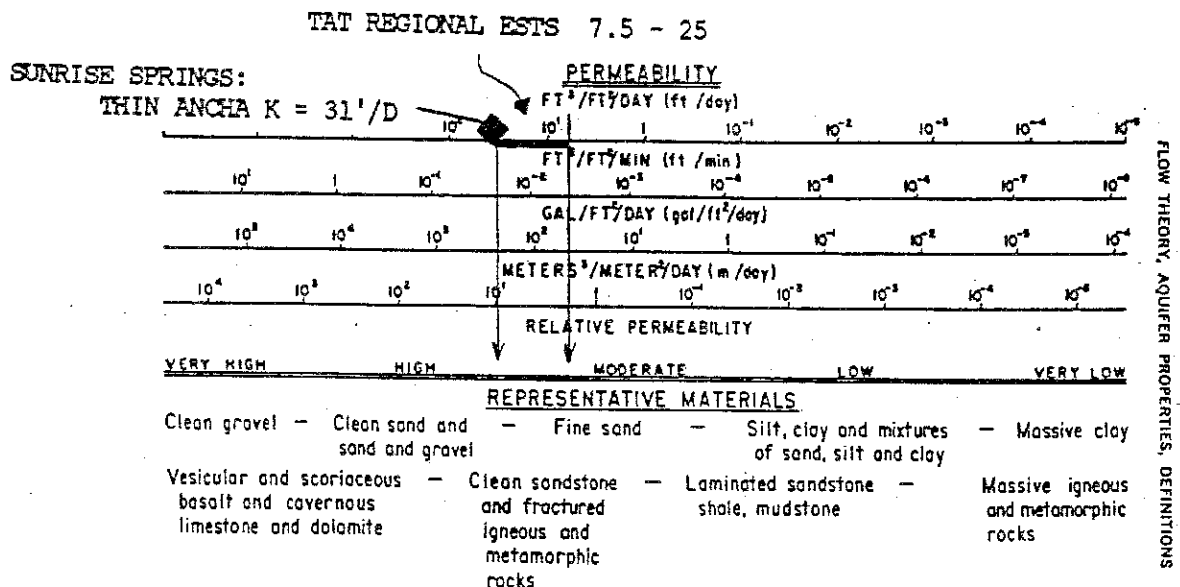


FIGURE 2-5.—Comparison of permeability and representative aquifer materials. 103-D-1407.

REPRESENTATIVE VALUES OF AQUIFER MATERIALS

Ta = ANCHA

Tt = TESUQUE

Tat = COMBINED VALUES

Sy = 0.05 - 0.20

Because strata of coarse, unconsolidated sediments underlie the valley, the area has been identified as being susceptible to groundwater contamination, particularly from septic tank effluent. In the 1980 Santa Fe County General Plan, the study area lies in a general outline of areas with potential man - made water pollution problems. However, most of the wells examined for this study report a 3 to 25 feet thick soil and clay near the surface, and many reported 10' to 30' of sandy clay above 60' drill depths. This stratification and the proposed well design should minimize the downward migration of any contaminants.

FINDINGS

Prototype Well Design

The objective of the following design is to isolate the Ancha aquifer and produce the underlying Tesuque Formation.

Based on 18 nearby wells the estimated deliverability is 10 to 15 gallons per minute (about half the average driller's estimate). The average well encountered the water table at about 64 feet and was drilled to 144 feet. About 25 feet of well casing was slotted or perforated at various depths. Very little information is reported on pump selection.

Utilizing generalized design considerations as well as conversations with Steve Kuckelman of Kuckelman Pump Services, the following features are estimated (Figure 5). The well should be drilled to 7 7/8" or greater in diameter, approximately 150 to 200 feet deep (i.e. have over a 100 foot water column), utilizing the mud rotary method. Five inch PVC casing should be installed, with more than 25' of slots opposite the most porous and permeable strata at least 50' below the water table.

Presuming the well is capable of pumping at 10 to 20 GPM, a 3/4 to 1 1/2 horse pump rated at 20 gpm, positioned at least 20 feet above total depth, should be sufficient for supplying up to four households.

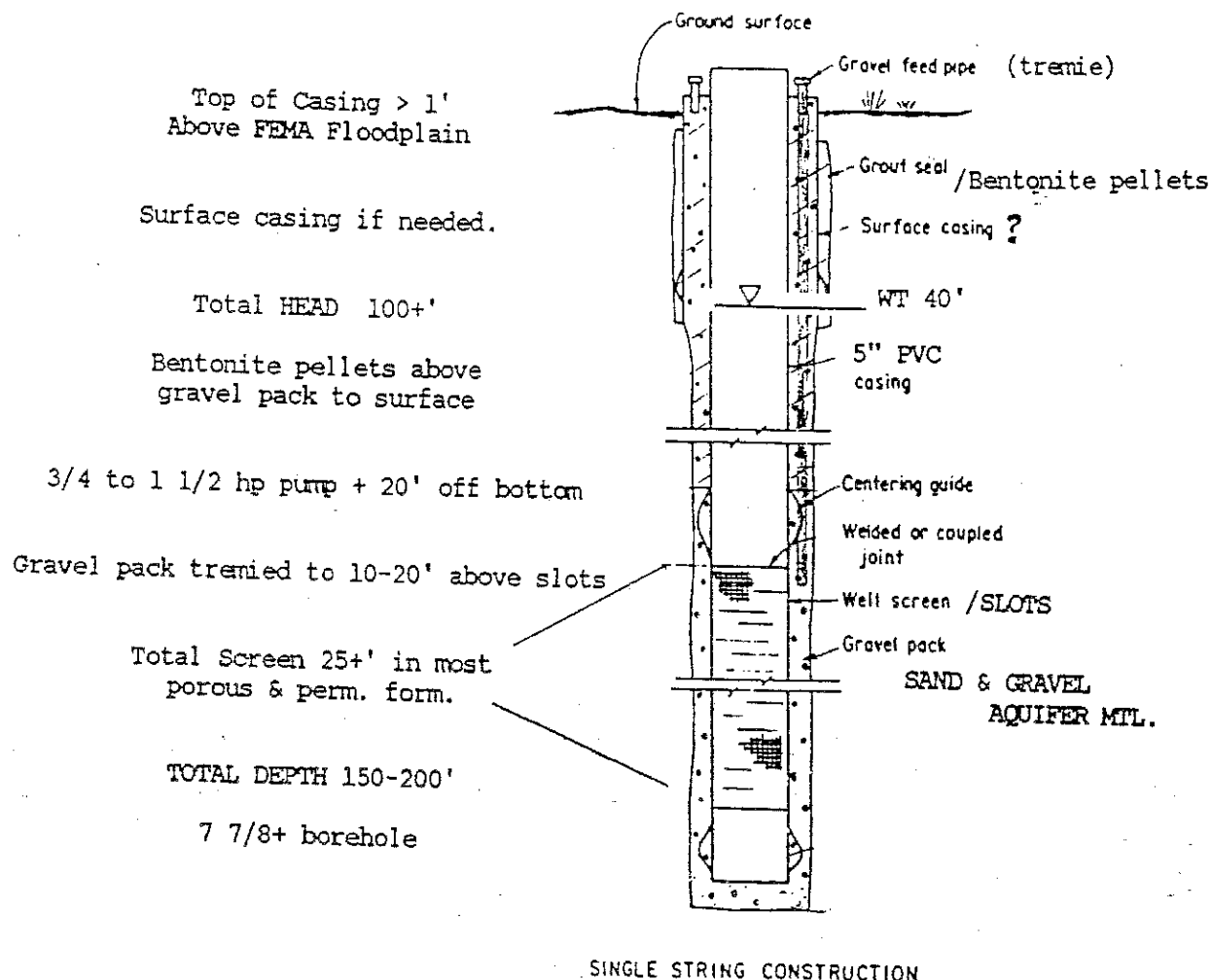


FIGURE 11-1.—Gravel packed, rotary drilled well for single string construction. 103-D-1488.

SUGGESTED PROTOTYPE WELL DESIGN
TO PRODUCE FROM THE TESUQUE FORMATION
AND ISOLATE THE ANCHA FORMATION

Prepared by: Jack P. Frost
Hydrogeologist
505-466-6435

Modified from the Ground Water Manual

A shared well system of this design should be able to serve up to 4 residences restricted to the County's 0.25 acre foot per year allowable. Shared wells will result in about 8 wells per 40 acre tract, versus 16 if each owner is responsible for their own well.

Because of the expected vertical stratification, wells should be perforated in the lowest permeable strata encountered to minimize downward induction of septic effluent. The annulus should be stabilized by gravel pack at least 10 feet above the top of perforations. Above the gravel pack pellet bentonite should be added to near ground level. In this way vertical flow in the borehole annulus will be minimized. This design is similar in some regards to precautions taken in the construction of ground water monitoring wells.

Drilling costs for the proposed design are estimated at \$16 to \$19 per foot (about \$2500 to 3800). The pump and surface equipment was estimated by Mr. Kuckelman at about \$4500 per well.

Mr. Kuckelman estimates that a four - home shared well system could reduce costs as much as 70 percent over single home well systems.

Well Drawdown Model

For comparison purposes, a well with a pumping rate of 0.60 gallons per minute (864 gpd or 1 acre foot per year), sufficient to serve 4 houses at a 0.25 af/yr allowable, has been modeled in Appendix 3. Actually, such a well typically produces it's average daily output in two to three hours of pumping per day. This translates into an actual, intermittent pumping rate of less than 8 gpm. Intermittent pumping causes a larger transient drawdown with interspersed periods of recovery. Such conditions and results should not be dissimilar to the model scenarios depicted in the Appendix.

The aquifer appears to be more than adequate for domestic use. To test the input assumptions, models were created using both the lower ($K=50$ gpd/ft, $S_y=.05$) and higher ($K=200$ gpd/ft, $S_y=0.15$) estimates of aquifer coefficients. The most conservative drawdown model indicates a maximum drawdown of less than 1 foot in the well bore and less than 0.2 feet at a radius of 100 feet, computed over a 40 year pumping interval.

Pollution Potential

Because the study area occupies the floodplain and is underlain by porous and permeable sediments, there is some concern for pollution potential. In a conversation with Mr. Gene Fulgenzi, Environmentalist at the District 11 office of the State E.D., he was unaware of any specific problems in the general area.

For the purposes of this study, no information was encountered regarding regional or point source contamination near or up gradient of the study area. Such potential sources include leaking buried tanks, agricultural chemical use or other subsurface disposal hazards.

Septic tanks, the means for domestic liquid waste disposal in this area, create an environment for bacteria to degrade domestic wastes. The effluent from the septic leach field is either transpired by plants or slowly makes its way downward to the water table. In this area the soils and bacterial action should remedial the effluent in a short distance, probably less than tens of feet. The horizontal stratification of the aquifer will also slow the downward percolation of the effluent.

The proposed well construction practices, as well as the natural filter function of the aquifer, should secure bacteria-free groundwater for many years. The State Environment Department specifies construction practices and setbacks from wells, and requires approval of individual septic tank systems.

SUGGESTED WELL LOCATIONS

Figure 6 is an orthographic survey plat of the Por Su Gracia Subdivision, showing suggested shared well sites. Approximately 9 sites are recommended, each to be shared by 2 to 3 lots and houses. These locations are based on topography and interpreted homesites. The average distance of water supply line is less than 250 feet. Final homesite choices might cause some adjustments to these suggestions, and some individual wells on the valley walls are likely because of rugged topography.

Considering the well design and model results described previously, well interference should not be an issue in this subdivision.

The following Table indicates lot locations and predicted drilling depths for shared wells located in Figure 6. The proposed depths should access the Tesuque Formation as the principle water bearing formation.

PROPOSED SHARED WELL SITES, ELEVATION, TOTAL DEPTH

Site	Lots Served B=Block, L=Lot#	Estimated Elevation	Estimated Total Depth (ft, app)
A	B2-L1,L2	6142	150+
B	B1-L1, L2	6136	150+
C	B1-L3,L4	6142	150+
D	B1,L3, L4?	6150	200+/-
E	B2-L5,L6	6154	200+/-
F	B1-L9?, L10,L11,L12	6160	200+/-
G	B1-L6,L7	6200	200



SUGGESTED SHARED-WELL LOCATIONS
FOR SU GRACIA SUBDIVISION

Prepared by: Jack P. Frost
Hydrogeologist
505-466-6435

- Computer models depict a modest impact on regional groundwater flow. The cones of depression will not interfere with one another to any significant degree. No impairment of prior ground water appropriators should be expected.
- If State approved practices are employed, the potential for local contamination from domestic septic tank systems appears minimal. The soils and horizontal stratification of the aquifer will remediate and impede downward - migrating contaminants.
- A shared well system, coupled with thoughtful well design and construction, will minimize the impact on the aquifer and ensure a safe water supply for the residents of the subdivision.

BIBLIOGRAPHY

AGW Consultants, 1986, Hydrogeology of Sunrise Springs Resort, Santa Fe County, New Mexico

Fleming, Bill, 1994, La Cienega Water Supply/Demand Analysis, Report prepared for Santa Fe County.

Spiegel, Z. And Baldwin, B., 1963, Geology and Water Resources of the Santa Fe Area, New Mexico, USGS Water Supply Paper 1525

Spiegel, Z., 1975, Preliminary Report on the Hydrology of the La Cienega Area, Santa Fe County N.M.: Consultant Report to Santa Fe Downs

Walton, W. C., 1987, Groundwater Pumping Tests, Design and Analysis, Lewis Publishers

APPENDICES

TABLE OF WELL RECORD INFORMATION

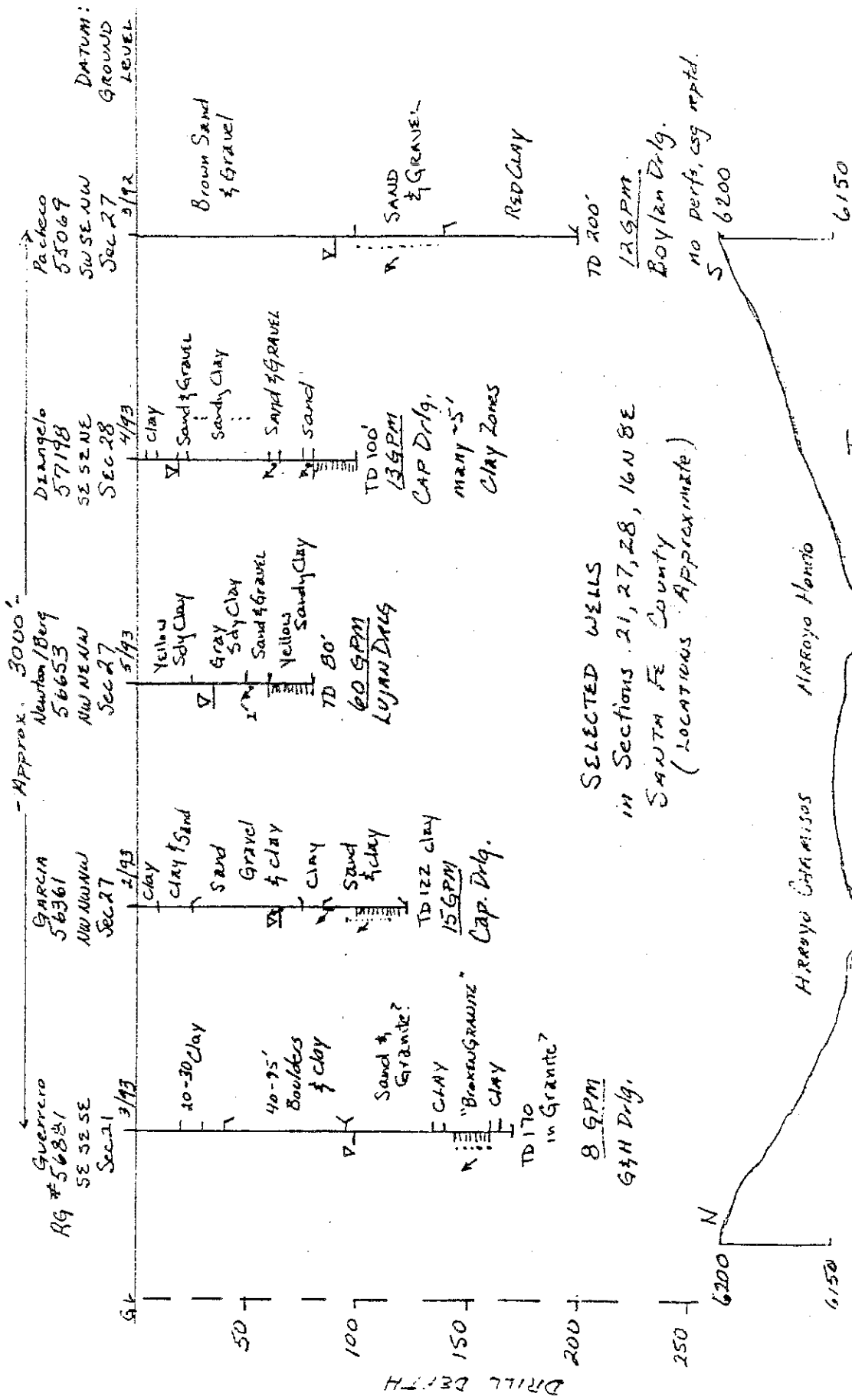
SCHEMATIC WELL LOG CROSS SECTION

PREDICTIVE MODEL USING HIGHER FORMATION COEFFICIENTS

PREDICTIVE MODEL USING MORE CONSERVATIVE COEFFICIENTS

TWO REPRESENTATIVE WELL RECORDS ADJOINING THE STUDY AREA

Well Number RG #	Owner, Location	Total Depth	Depth to Water	Yield (GPM)	Water Column	Depth to Base of Low Zone	Principle Water Bearing Formation	Perfs, Casing	Drilling Contractor
56881	SE,SE,SE,21	170	100	89	70	160	Pink Bkn Granite	20, 5" pvc	G & H
21468	SE,SW,SW,22	72	28	NR	44	68	Brown-Red SD	23, 6.625"	Crocker
56653	NW,NE, NW,27	80	35	60	45	52	Yel. Sand & Gravel	20, 6.625"	Lujan
56361	NW,NW,NW,27	122	65	15	57		Sand & Gravel	20, 5"	Nuanes (Cap)
55069	SW,SE,NW,27	200	90	12	110		Sand & Gravel (poor)	40, 7.875" hole	Boylan
56348	SE,NE,NE,28	165	40	20	125		Red Grav., Blue Clay & Gravel	30, 4.5" pvc	Garcia
57198	SE,SE,NE,28	100	19	13	81		Sand, Sand & Gravel	20	Nuanes (Cap)
58393	SE,SE,NW,22	108	64	20	42	95	Sand & Gravel	20, 5"	Nuanes (Cap)
58245	SE,SE,NW,22	117	69	20	48	44	Sand & Gravel	20, 5"	Nuanes (Cap)
58411	SW,SE,22	105	61	20	44		Gravel	20, 5"	Nuanes (Cap)
55880	SE,NW,SW,27	200	80	20	120	75	Layers of Sand & Gravel	40, 5.5"	Boylan
55355	NW,NE,SW,27	200	100	10	100		Red & White Clay & Rock	30, 4.5"	Garcia
55154	NW,NE,SE,28	90	33	20	57		Sand & Gravel	20, 5"	Nuanes
41553	SW,SE,SW,22	100	42	15	58		Sand, Sand & Gravel	20, 6.625"	Roybal
41775	SE,SE,SW,22	373	125	150	248	370	Brown Sand & Gravel	113, 6.625"	Boylan
42782	NW,SE,NW,28	90	20	20		80	Gray Silt	20, 6.625"	Boylan
56898	SW,NE,NE,28	160	99	20		53	Sand & Gravel	20, 5"	Nuanes
56178	PERMIT ONLY								
57760	NE,NE,SE,28	145	75	7		120	"Wash & Boulders	50, 4.5"	Thompson
AVERAGES		144.3	63.6	31.2	83.3	111.8			



SELECTED WELLS
in Sections 21, 27, 28, 16N 8E
SANTA FE County
(Locations Approximate)

Program: PT1
Version: IBM/PC 2.1
Model : SIMULATION OF 1 OR 2-LAYER AQUIFER SYSTEM,
UNIFORM PROPERTIES, WELL STORAGE CAPACITY,
DELAYED GRAVITY YIELD, LEAKAGE, DEWATERING,
RADIAL FLOW TO PRODUCTION WELL, FINITE-
DIFFERENCE APPROXIMATION FOR PUMPING TEST
DESIGN

Program based in part on program presented
by Rushton, K.R. and S.C. Redshaw. 1979. Seepage
and groundwater flow-numerical analysis by
analog and digital methods. John Wiley & Sons, Ltd.
New York; and Rathod, K.S and Rushton, K.R. 1984.
Numerical method of pumping test analysis using
microcomputers. GROUND WATER. Vol. 22, No. 5.

DATA BASE:

AQUIFER HORIZ. HYDR. COND. (GPD/SQ FT)= 200.00
AQUIFER VERT. HYDR. COND. (GPD/SQ FT)= 20.000
AQUIFER THICKNESS (FT)= 100.00
ARTESIAN AQUIFER STORATIVITY (DIM)= 1.0000D-03
WATER TABLE STORATIVITY (DIM)= 0.1500
PRODUCT. WELL EFFECTIVE RADIUS (FT)= 0.400
TOP OF AQUIFER DEPTH (FT)= 50.00
BASE OF AQUIFER DEPTH (FT)= 150.00
INITIAL WATER LEVEL DEPTH (FT)= 50.00
INFINITE AQUIFER SYSTEM

COMPUTATION RESULTS:

PRODUCTION WELL DISCHARGE RATE (GPM)= 0.60

PRODUCT. WELL EFFECTIVE RADIUS (FT)= 0.400

TIME AFTER PUMPING STARTED (MIN)= 21024000.00

DISTANCE-DRAWDOWN OR WATER LEVEL VALUES AT END OF PUMPING PERIOD

NODE NO	RADIUS (FT)	DRAWDOWN OR WATER LEVEL (FT)	
2	0.40	50.08	
3	0.63	50.07	
4	1.00	50.07	
5	1.59	50.07	
6	2.52	50.06	
7	4.00	50.06	
8	6.34	50.06	
9	10.05	50.05	
10	15.92	50.05	
11	25.24	50.05	
12	40.00	50.04	
13	63.40	50.04	
14	100.48	50.04	
15	159.24	50.03	
16	252.38	50.03	
17	400.00	50.03	
18	633.96	50.02	
19	1004.75	50.02	
20	1592.43	50.02	
21	2523.83	50.02	
22	4000.00	50.01	
23	6339.57	50.01	
24	10047.55	50.01	
25	15924.29	50.00	
26	25238.30	50.00	

PREDICTIVE MODEL OF DRAWDOWNS
HIGH K, Sy EXAMPLE
40 YEAR INTERVAL

DATA BASE:

AQUIFER HORIZ. HYDR. COND. (GPD/SQ FT)= 50.00
 AQUIFER VERT. HYDR. COND. (GPD/SQ FT)= 5.000
 AQUIFER THICKNESS (FT)= 100.00
 ARTESIAN AQUIFER STORATIVITY (DIM)= 1.00000D-03
 WATER TABLE STORATIVITY (DIM)= 0.0500
 PRODUCT. WELL EFFECTIVE RADIUS (FT)= 0.400
 TOP OF AQUIFER DEPTH (FT)= 50.00
 BASE OF AQUIFER DEPTH (FT)= 150.00
 INITIAL WATER LEVEL DEPTH (FT)= 50.00
 INFINITE AQUIFER SYSTEM

COMPUTATION RESULTS:

PRODUCTION WELL DISCHARGE RATE (GPM)= 0.60

TIME AFTER PUMPING STARTED(MIN)=21024000.00

DISTANCE-DRAWDOWN OR WATER LEVEL VALUES AT END OF PUMPING PERIOD

NODE NO	RADIUS(FT)	DRAWDOWN OR WATER LEVEL (FT)
2	0.40	50.30
3	0.63	50.29
4	1.00	50.27
5	1.59	50.26
6	2.52	50.25
7	4.00	50.23
8	6.34	50.22
9	10.05	50.21
10	15.92	50.20
11	25.24	50.18
12	40.00	50.17
13	63.40	50.16
14	100.48	50.15
15	159.24	50.13
16	252.38	50.12
17	400.00	50.11
18	633.96	50.09
19	1004.75	50.08
20	1592.43	50.07
21	2523.83	50.06
22	4000.00	50.04
23	6339.57	50.03
24	10047.55	50.02
25	15924.29	50.01
26	25238.30	50.00

PREDICTIVE MODEL USING LOW-END
VALUES OF K, Sy

**STATE ENGINEER OFFICE
WELL RECORD**

Section 1. GENERAL INFORMATION

Owner of well DONNA DEANGELO Owner's Well No. _____
 Street or Post Office Address 992 Ave. Las Campanas
 City and State Santa Fe, NM

Well was drilled under Permit No. RG 57198 and is located in the:

a. 1/4 SE 1/4 SE NE 1/4 of Section 28 Township 16N Range 8E N.M.P.M.

b. Tract No. _____ of Map No. _____ of the _____

c. Lot No. _____ of Block No. _____ of the _____
 Subdivision, recorded in Santa Fe County.

d. X= _____ feet, Y= _____ feet, N.M. Coordinate System _____ Zone in the _____ Grant.

(B) Drilling Contractor Capitol Drilling License No. WD 1004

Address Rt 8, Box 331N, Santa Fe, NM 87505

Drilling Began 4-27-93 Completed 4-27-93 Type tools Rotary Size of hole 7 7/8 in.

Elevation of land surface or _____ at well is _____ ft. Total depth of well 100 ft.

Completed well is ☒ shallow ☐ artesian. Depth to water upon completion of well 19 ft.

Section 2. PRINCIPAL WATER-BEARING STRATA

Depth in Feet		Thickness in Feet	Description of Water-Bearing Formation	Estimated Yield (gallons per minute)
From	To			
19	22	3	Sand & Gravel	
60	65	5	Sand & Gravel	13 Total
75	80	5	Sand	

Section 3. RECORD OF CASING

Diameter (inches)	Pounds per foot	Threads per in.	Depth in Feet		Length (feet)	Type of Shoe	Perforations	
			Top	Bottom			From	To
5	2.48		0	100	100	NONE	80	100

Section 4. RECORD OF MUDDING AND CEMENTING

Depth in Feet		Hole Diameter	Sacks of Mud	Cubic Feet of Cement	Method of Placement
From	To				

MAY 7 1993
 ALBUQUERQUE, N.M.
 P.I.: 118
 OFFICE

1027
 STATE ENGINEER OFFICE
 ALBUQUERQUE, N.M.

STATE ENGINEER OFFICE
 ALBUQUERQUE, N.M.
 MAY 7 1993
 121

Color and Type of Material Encountered 5/198			
From	To	in Feet	
0	3	3	Sandy Clay
3	5	2	Sand & Gravel
5	10	5	Clay
10	11	1	Sand & Gravel
11	18	7	Clay
19	22	3	Sand & Gravel
22	30	8	Clay & Sand
30	39	9	Clay
39	60	21	Sandy Clay
60	65	5	Sand & Gravel
65	66	1	Clay
66	70	4	Sandy Clay
70	71	1	Sand
71	75	4	Clay
75	80	5	Sand
80	85	5	Clay
85	90	5	Sandy Clay
90	93	3	Sand
93	94	1	Sandy Clay
94	99	5	Sand
99	100	1	Clay

Section 7. REMARKS AND ADDITIONAL INFORMATION

STATE ENGINEER OFFICE WELL RECORD

Section 1. GENERAL INFORMATION

Owner of well Helen P. Newton / Terry Berg Owner's Well No. 93 JUN 7 AM 10-26
Street or Post Office Address Rt. 14, Box 200
City and State Santa Fe, NM 87501

was drilled under Permit No. RG-56653 and is located in the: STATE ENGINEER OFFICE SANTA FE NEW MEXICO

a. 1/4 NW 1/4 NE 1/4 NW 1/4 of Section 27 Township 16N Range 8E N.M.P.M.

b. Tract No. _____ of Map No. _____ of the _____

c. Lot No. _____ of Block No. _____ of the _____
Subdivision, recorded in Santa Fe County.

d. X= _____ feet, Y= _____ feet, N.M. Coordinate System _____ Zone in the _____ Grant.

Drilling Contractor Lujan Drilling License No. WD-547

Address Rt. 3, Box 95-78, Santa Fe, NM 87505

Drilling Began 5-14-93 Completed 5-14-93 Type tools Rotary Size of hole 9 in.

Elevation of land surface or _____ at well is _____ ft. Total depth of well 80 ft.

Drilled well is ☒ shallow ☐ artesian. Depth to water upon completion of well 35 ft.

Section 2. PRINCIPAL WATER-BEARING STRATA

Depth in Feet		Thickness in Feet	Description of Water-Bearing Formation	Estimated Yield (gallons per minute)
From	To			
50	52	2	Yellow Sand & Gravel	60 ?

Section 3. RECORD OF CASING

Diameter (inches)	Pounds per foot	Threads per in.	Depth in Feet		Length (feet)	Type of Shoe	Perforations	
			Top	Bottom			From	To
6 5/8			0	80			60	80

Section 4. RECORD OF MUDDING AND CEMENTING

Depth in Feet		Hole Diameter	Sacks of Mud	Cubic Feet of Cement	Method of Placement
From	To				
10	12				
12	14				
14	16				

[illegible]

JACK PHILIP FROST

GEOLOGIST, HYDROLOGIST
(505) 466-6435

RT. 3 BOX 95-37
SANTA FE, NM 87505

Transmittal Letter

To: Mr. Charles Heaton
Mr. Joe Catanach
Santa Fe County Land Use


September 28, 1994

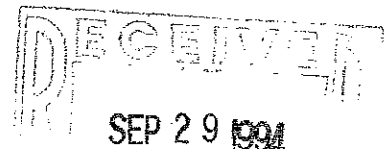
Re: Vista de Sandia Subdivision

Enclosed is an addendum to the hydrogeologic study I prepared for the aforementioned subdivision. Please include this in the submittal package for the project. I find sufficient water availability to support 2.5 acre development in the area.

Would you please review the attached addendum and call me if you have any questions? My investigations in this area are ongoing, and I will promptly notify you of any new or revised findings. Feel free to call me if I can be of any assistance.

Sincerely,


Jack P. Frost



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ADDENDUM TO HYDROGEOLOGIC REPORT

Re: Por Su Gracia , Vallecitas de Gracia, and Vista de Sandia Subdivisions

Calculations of Water Availability beneath 2.5 acre tracts in Subject Area.

Prepared by Jack P. Frost, Hydrogeologist

This memo supplements the hydrologic studies I have prepared in sections 21, 22, 27, and 28, T16N, R8E, Santa Fe County. As mentioned in the reports, there are a number of pumping tests in the area, to the east at the Racetrack, to the southeast at La Canada Subdivision, and to the west at Sunrise Springs. The findings of hydraulic coefficients from these tests are characteristic of the Ancha and Tesuque formation aquifers. Sample and geophysical logs for a uranium test hole beneath the subject area are attached, demonstrating the presence of a thick section of saturated Tesuque aquifer. I believe the Ancha-Tesuque contact occurs at about 70 feet in this well. Permeable Tesuque sands occur at 120', 160, and 200' which are suitable for a domestic well completion.

A calculation of the County Code-prescribed Water Availability follows. This calculation is based on the generalized well design proposed, having total depth of 200 feet and a Saturated Thickness of 135'. A 100 year availability of 0.1134 acre foot per acre per year is calculated. This results in an availability beneath a 2.5 acre tract of 0.2835 acre feet per year. The County permits 2.5 acre densities with a restriction on water use of 0.25 acre feet per year in this area. Again, the wells in this area could be drilled deeper to demonstrate greater availability, but this would be unnecessary. The average depth of 18 domestic wells in the immediate vicinity is 144 feet.

Also attached is a revised computer flow model demonstrating the predicted drawdowns pumping 1 acre foot per year for 100 years (allowable for 4 lots sharing the well). Conservative coefficients were used in this calculation, and it demonstrates a modest drawdown of less than 2 feet at radii greater than 160' from the modeled well. According to this model well interference will be negligible. This model does not consider the presence of many hundreds of feet of Tesuque formation not penetrated in the proposed well design.

If you have any questions about these findings please call me at 466-6435.