TABLE 1

denotes wells adjoining the study area

Well	Owner	Location	Date	Total	Depth to Water	Yield	Water	Depth to	Depth to	Estimated	Water	Principal Water Bearing Formation	Drilling
			!			7			Low Zone		(Fw		5
. 56348	Case	SE NE NE, 28	Nov-92	. 165	40	20	125	40	165			Red Gravel and Blue Clay	Garcia's
56361	Garcia	Garcia NW,NW,NW,27	Feb-93	122	65	15	57	96	115			Snd & Grvl 65-75, Snd & Grvl 85-90, Sand 96-115	Nuanes-Cap
55069	Pacheco	Pacheco SW,SE,NW,27	Mar-82	200	. 90	12	110	100	140			Sand and Gravel	Boylan
56653	Newton	Newton NW,NE,NW,27	May-94	80	35	90	45	20	52			Yellow Sand and Gravel	Lujan
57198	Deangelo	SE,SE,NE,28	Apr-93	100	19	13	81	75	90			Snd & Grvl 19-22, Snd & Grvl60-65, Sand 75-80	Nuanes-Cap
58393	Gallegos	SE,SE,NW,22	Oct-93	108	64	20	44	64	95			Sand and Gravei	Nuanes-Cap
58245	Montoya	SE,SE,NW,22	Oct-93	117	69	20	48	69	117			Sand and Gravet	Nuanes-Cap
/ 56881	Guerro		Mar-93	170	100	8	70	145	160			Pk Bkn Granite	G&H
21468		SE,SW,SW,22	Aug-72	72	28		44	59	69			Brn, Red Sand	Crocker
56653			May-93	80	35	9	45	50	25		ļ 	Yel. Sand & Gravel	Lujan
56361		NW,NW,NW,27	Feb-93	122	65	15	57					Sand and Gravel	Nuanes-Cap
55069		SW,SE,NW,27	Mar-92	200	06	12	110					Sand and Gravel (poor)	Bovlan
1.56348		SE,NE,NE,28	Nov-92	165	40	20	125					Red Grav., Blue Clay and Gravel	García
57198		SE,SE,NE,28	Apr-93	100	19	13	81					Sand, Sand and Gravel	Nuanes-Cap
58393	Gallegos	SE,SE,NW,22	Oct-93	108	64	20	44	5	95			Sand and Grave	Nuanes-Cap
58245	Montoya	SE, SE, NW, 22	Oct-93	117	69	250	48		44			Sand and Gravel	Nuanes-Cap
58411	Gallegos	SW,SE,22	Oct-93	105	61	20	44					Gravel	Nuanes-Cap
55880	Holmes	Holmes NE,NW,SW,27	Sep-92	200	90	20	120	25	52			Layers of Sand and Gravel	Boylan
55355	Romero	Romero NW,NE,SW,27	May-92	200	100	10	100					Red and White Clay and rock	Garcia
55154	Madrid	Madrid NW,NE,SE,28	Apr-92	06	33	20	57					Sand and Gravel	Nuanes-Cap
41553	Gallegos	Gallegos SW, SE, SW, 22	Apr-84	100	42	15	58				İ	Sand, Sand and Gravel	Roybal
41775	Cook		May-84	373	125	150	248	120	370			Brown Sand and Gravel	Boylan
. 42782	Pino	NW,SE,NW,28 Nov-84	Nov-84	96	20	20	70	20	90			Gray Sitt	Boylan
26898	McNeil	SW,NE,NE,28	Apr-93	160	99	50	61		53			Sand and Gravel	Nuanes-Cap
56178			Sep-92				0			•		55.	
57760		NE,NE,SE,28	Jul-93	195	75	7	120		120			Wash and Boulders	Thompson
21469	Quintana	SE,SW,SW,22	Aug-72	72	28	ļ	44	31	69			Brn/Red Sand	Crocker
1			1										
												TO THE PARTY LAST C. LAST CO. C.	1 5 miles
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				+				,			-		:
			Ī									AND THE RESIDENCE OF THE PARTY	:
Averages:				139	09	35	76	29	108				
					_								

Vicinity of Section 21 T16N, R8E Prepared by Jack P. Frost July 1, 1994

# STATE ENGINEER OFFICE WELL RECORD

			Section 1.	GENERAL IN	FORMATION		*92 as	
		<del></del>		Gerardo	Guerrero	Owner	's Well No. 7	2
(A) Owner or	Well(#### Post Office Add	dress181	7 Mann	St			STATE	<u>_#/7_10</u>
City and	State	Santa	Fe N M	87501			SANTA ENGI	iiFED .
Well was drilled	under Permit !	\$6. <u>RG-5</u> 6	881		and is located	Owner	TEN	EW MEXIC
s. SE	4 <u>SE</u> 4	SE %_	¼ of Sec	tion <u>21</u>	Township1	.6N Ran	ge <u>8E</u>	N.M.P.M.
b. Tract	No	_ of Map No.		of the				
c. Lot No	ovision, recorded	of Block No I inSAN	TA FE	of the	ounty.	<u></u>		
d. X=		_ feet, Y=		feet, N.	M. Coordinate S	System		Zone in Grant.
(B) Drilling C	Contractor <u>G8</u>	H Brill	ing $_{arphi}$	retty acc	7 1	_ License No	WD 815	
			7	•			•	•
Drilling Began	3/5/93	Com	pleted 3/9	9/93	_ Type tools	Rotary	Size of hole_	7 7/8 in.
						_ ft. Total depth		
Completed wel	1:a 🔽 a	nallow []	ortecian		Depth to water	upon completion	of well 100	ft.
Completed wet	112 127 21				R-BEARING ST			
Danah	in East		<del></del>	CIFAL WAIL	K-BEARING ST	RATA .	Estimated	Yield
From	in Feet To	Thickness in Feet	s l	Description of	Water-Bearing F	ormation	(gallons per	
145	160		P	ink boke	n granite		about 8	
								-
							,	
			Sectio	n 3. RECORD	OF CASING			,
Diameter	Pounds	Threads	Depth	in Feet	Length	Type of Sho	Perfe	orations
(inches)	per foot	per in.	Тор	Bottom	(feet)	1,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	From	То
5	PVC		1½	170	171½	OPen	150	170
		Sec	tion 4. RECO	RD OF MUDI	NING AND CEM	IENTING	<u> </u>	
Depth From	in Feet To	Hole Diameter	Sac of M		Cubic Feet of Cement	<u> </u>	od of Placement	
						2 2 2	20	
						₹0.2  -	ੁੱ ਜ	92
	T					74	37	

То	in reet	
		56881
10		Laure Gravei & Bouldars
20		Bouldnra
30	10	Clay
40		
95	± 55	Bouldars & Clay ? Base Ancha?
135		Pink Sand & Granite
140	5	Clay
160		Swad & Grantite
185	5	Clay
170		Oranica ?
i		·
	10 20 30 40 95 135 140 160 165 170	10 20 30 10 40 95 ±55 132 140 5 160 165 5

Section 7. REMARKS AND ADDITIONAL INFORMATION

### WELL RECORD

INSTRUCTIONS: This form should be executed in triplicate, preferably typewritten, and submitted to the nearest district office of the State Engineer. All sections, except Section 5, shall be answered as completely and accurately as possible when any well is drilled, repaired or deepened. When this form is used as a plugging record, only Section 1A and Section 5 need be completed.

Section 1			_ (A) Owne	er of well.	GAR	1 90107	ANA	
		, [	Street and	Number.	RT 4	4 BOX C	74	
			City S	1 <i>NTA</i> _	FE_		State L	M
			Well was	drilled un	der Perm	it No. RG 21:	468 and	is located in the
		1	SEV	SW 4	SW 4	of Section 22	Twp. 16-1	J Rge 8-€
			B) Drilli	ing Contra	ctor C.P.	OCKER;	INC Licen	se No. WO- 214
			Street and	l Number	RT 4	BOX 9	4 5	<u> </u>
-			City SA/	VTA E	=	,	State _/	UM.
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	. 1		Drilling w	as comple	tedA	0629		19.72
(Pl	lat of 840 ac	res)				<b>27</b>		2 /
Elevation	at top of	casing in f	eet above se	a level	24	lotal dep	oth of well. 7: er upon complet	78:
State whe	ether well	is shallow	or artesian.	SELECT	C.W	Depth to wat	er upon complet	
Section 2			PRIN	CIPAL WA	TER-BEAR!	NG STRATA		977
No.	Depth in	Feet 2	hickness in		Des	cription of Water	-Bearing Formation	(T)
	From	То	Feet	<u> </u>				<u> </u>
1	3/	5/	<del>20</del> .			SAND		[ 2 ]
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4			'				-	₽ <b>25</b>
5				7				i <del>-</del>
Section 3		!	1	PECOP	D OF CAS	ine.		
		1 -			1	i	Perfo	rations
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Section 5	ia (a.	r v.	4.	, PLUG	SING REC	ORD	T. T. N. T.	ш.
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	d Number				_ City	<del>,</del>	State	
Tons-of (	Clay used ,		Tons of R	oughage i	ised:	Ty	pe of roughage	
Plugging	method us	ed				Date Plu		19
Plugging	approved	by: i	. 1 52	1	1	Cement Plug	gs were placed as	s follows: :
, <del>, , , , , , , , , , , , , , , , , , </del>	· 			· <u>·</u> ···	No	Depth of P	No. o	f Sacks Used
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	FOR USE	OF STATE	engineer o	NLY				
						<del> </del>		
Date I	Received		<del>t- 338-71</del>	1.				
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File No.	RG-	21468	<u> </u>	UseC	la m	Locatio	n No. 16.8.	₹ <i>₹</i> .334

Date Book has

Section 6

LOG OF WELL

ection 6		100	LOG (	# WELL	
· Depth From	in Feet To	Thickness - in Feet	Color	Type of Material Encountered	-i -i
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23	3/_	8	BROWN	SANDY CLAY	
37	:51	20	//	SAND (WATER)	
51,	59.	පි,	//	SANDY CLAY BOULDERS	
59	69	10	BROWN/ RED	SAND- (WATER)	
69	72	3/	₽ <b>∈</b> D	CLAY	
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<u>4</u>			· · · · · · · · · · · · · · · · · · ·		
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· ' ' '	0.4 36	. The first	7 ft East 1.7	Wint wind & Hall XX	,

The undersign	ned hereby cert	ifies that, to the best of his	knowledge and belief, the	ne foregoing is a true, and co
rect record of	the above desc	ribed well	Vice Sa.	ia √•Û
:	1	CHA TO LEA	2000	and Comment
- '	,	City 547/771 62	-Zdisiu	in Existing
	•	Street and Gimmer PT	4 Kill F City	n Driffer
	i	(B) Drilling t settingers?	UCCK#347 30 0	g " in with the CD 21d
1	1 :			WO 1/2 1 RES. 6 - F-
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•	1	1914 SANZA 15.	·	2005 G 1 V 1 1 1 1 1
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i	· · · · · · · · · · · · · · · · · ·	(A) Derver of well Cafe.	( 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	

Section 1 ... CAREN GOILL

WELL PROCAD

şe 2 31

THE REPORT OF THE STEELINGS

# STATE ENGINEER OFFICE

# WELL RECORD

### Section 1. GENERAL INFORMATION

	of well	He	len P. Ne	wton / Ter	ry Berg	93 J	's Well No.	<u> </u>
	d State	Sa	nta Fe, N	M 87501		<del>- ਪਰ ਹ</del>	UN 7 AM 1	n 20
		-	F / / F 3			1 in the: 57.77.	C. E. C. Commission	
b. Trac	t No.	of Map No		of the				
c. Lot Subs	No livision, recorded	of Block No I inS	anta Fe	of the	ounty.			
		•		feet, N.	M. Coordinate	System		
(B) Drilling	Contractor	L	ujan Dril	ling		License No. WD	-547	
Address		R	t. 3, Box	95-78, Sa	nta Fe, N	1 87505		
Drilling Begat	5-14-93	Com	pleted <u>5-1</u>	4-93	_ Type tools	Rotary	Size of hole_	<u>9</u> in.
Elevation of i	and surface or _	· ·		at we	l is	ft. Total depth	of well	80 ft.
Completed w	ئو 🔀 عا الع	wollan			Depth to water	r upon completion	of well	35
Depti	in Feet	Thickness	. 1				Estimated	Yield
From	То	in Feet	ľ	escription of	Water-Bearing	Formation	(gallons per s	
50	52	2	Yel	low Sand &	Gravel		6	0 0
				· · · · · · · · · · · · · · · · · · ·		<u> </u>	·	
			Section	n 3. RECORD	OF CASING			
Diameter	Pounds	Threads	Depth		Length (feet)	Type of Shoo	<u> </u>	rations
(inches) 6 5/8	per foot	per in.	<u>Тор</u> О	Bottom 80	(teet)		From 60	80
				Andrews (Control of the Control of t			, .	
	7 - 3	. Sect	ion 4. RECO	RD OF MUDD	ING AND CEN	MENTING	·	
Depti From	in Feet 3	X Hole	Sack of Mi		ubic Feet Cement	Metho	d of Placement	<i>'</i>
		z z				i	25	
	<b>a</b> . 36	אנור. י					E A	96.
	82	2				ř	२० <b>७</b>	

•	To	in Feet	Color and Type of Material Encountered 56653
0	25	25	Yellow - Sandy Clay
25	50	25	Gray - Sandy Clay
		10	
50	60		Yellow - Sandy Clay D 5
60	80	20	Yellow - Sandy Clay Px 5
<u> </u>			
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Section 7. REMARKS AND ADDITIONAL INFORMATION

WATER RESOURCE STUDY AND WELL DESIGN

POR SU GRACIA SUBDIVISION

SECTIONS 27 AND 28, T16N, R8E

SANTA FE COUNTY, NEW MEXICO

Prepared by: Jack P. Frost

Hydrogeologist

505-466-6435

January, 1994

Revised June, 1994

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FIGURE 3, REGIONAL CROSS SECTION	5
HYDROGEOLOGIC SETTING	6
Springs in the Area	7
Aguifer Properties	8
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APPENDICES

### PRE-DRILL REVIEW

### POR SU GRACIA SUBDIVISION

### WATER RESOURCE STUDY AND WELL DESIGN

SECTIONS 27 AND 28, T16N, R8E, SANTA FE COUNTY, N.M.

Prepared by: Jack P. Frost
Hydrogeologist
June, 1994

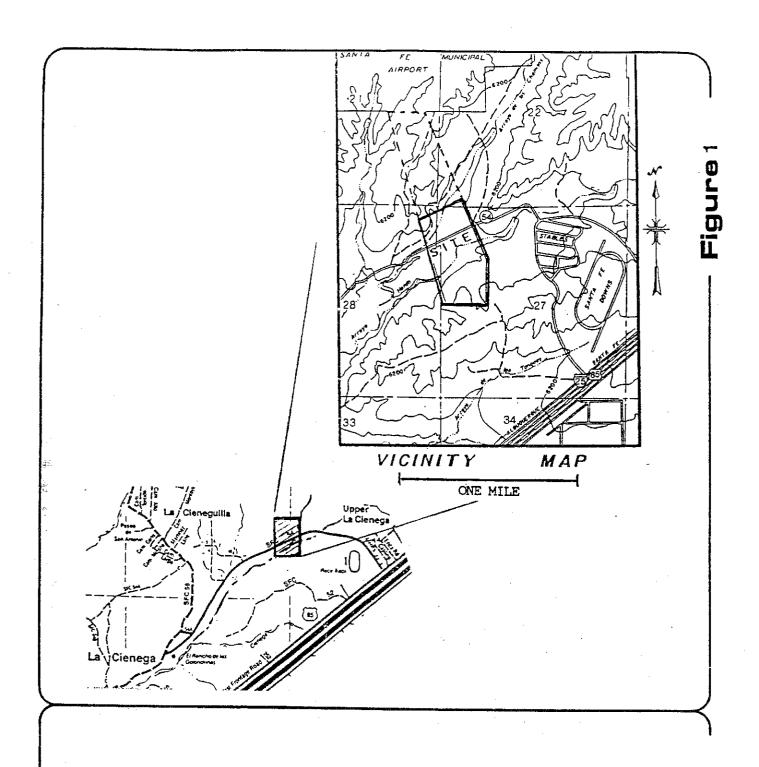
### INTRODUCTION

This report reviews the hydrogeology in the vicinity of two adjoining forty acre tracts near La Cienega, Santa Fe County. Also included is a plan for a typical well design and distribution of shared wells. The owners propose to subdivide the parcels into approximately 2 1/2 acre tracts.

The premise of this study is that a shared well system, coupled with thoughtful well design and construction, will be economical and will minimize the impact on the shallow aquifer. Such a system will ensure a safe water supply for the future.

This study shares several features of the County Code - prescribed Hydrogeologic Report. The owners are not asking for increased lot density. It is their intent to adopt the 2 1/2 acre density allowed by the County Code in this area when dwellings are restricted to 0.25 acre feet per year of water, including water conservation measures.

The study area lies in the County's Extra - Territorial Zone, in the Basin Hydrologic zone. It flanks County Road 54 approximately 1 1/4 miles from the intersection with Racetrack Road. It lies west of the Santa Fe Downs race track in the valley of the confluence of Arroyos Chamiso and Hondo {Figure 1}.



LOCATION OF THE POR SU GRACIA
AND BROWN TRACTS, SANTA FE COUNTY

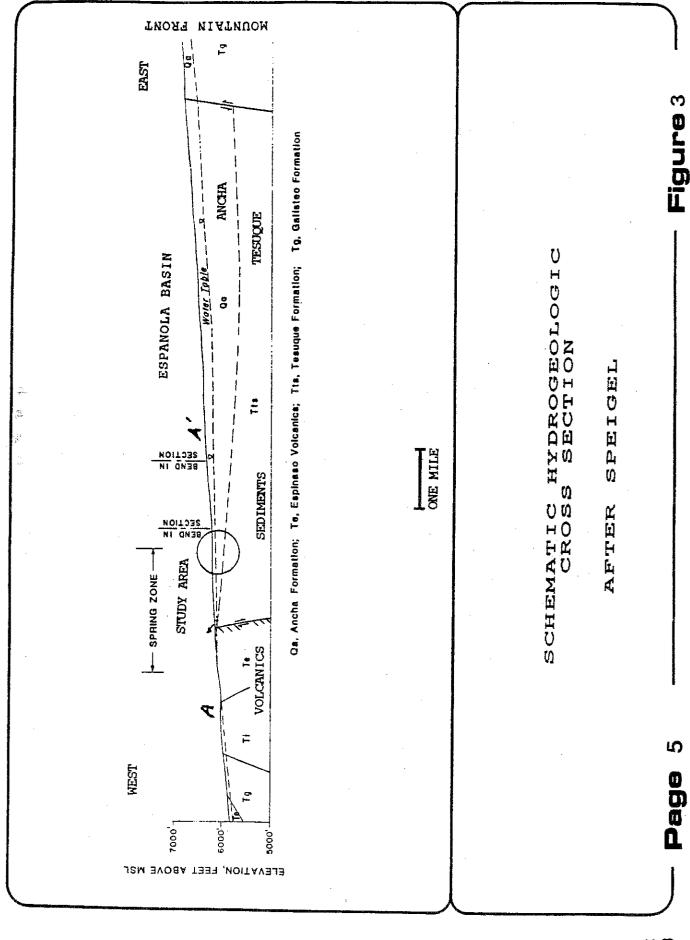
SCOPE

The scope of this project is a departure from common practices in the area. Typically individual landowners have drilled single - dwelling wells with little consideration of impact or contamination potential. From the review of well logs it appears that drillers' completion practices are highly varied.

Approximately 18 wells within a one - half mile radius were reviewed in this study. Over 90 wells and/or permits are on file at the State Engineer's Office within a one mile radius of the subject tract. From the well logs a cross section was constructed (Appendix 2) and the subsurface hydrogeologic conditions were interpreted. The well logs have also been helpful in designing a prototype well whose construction should protect the shallow Ancha Formation aquifer as well as minimize contaminant susceptibility from septic tank and other surface sources.

Several regional studies serve as important references for this report. They include Spiegel and Baldwin, 1963; and Fleming, 1994. Locally, several studies have been prepared to evaluate development at the Racetrack (Spiegel, 1975), and at Sunrise Springs Resort (AGW Consultants, 1976).

In order to optimize the number and distribution of shared wells on the property several computer models have been constructed to simulate drawdown and potential interference in the well field.



### HYDROGEOLOGIC SETTING

The hydrogeologic setting of the study area is depicted in Figures 2 and 3. They are modified from the AGW Consultants' study at Sunrise Springs Resort.

The study area lies on the west flank of the Espanola Basin. The older Tesuque and Ancha Formations, and recent basin -fill sediments terminate against a fault about a mile west of the study area (Spiegel, 75). Relatively impermeable volcanic rocks adjoin the fault zone on the west, creating a groundwater flow boundary. Ground water flows westward from the mountains, and the water table "piles up", in effect, against the volcanic rocks and discharges through springs, streambeds and phreatophytes in the vicinity (Figure 3).

The subject tracts occupy the floodplain and flanking hillsides of Arroyos Chamisa and Hondo. The arroyos are underlain by alluvial sand and gravel, silt and clay derived from the mountains to the east. These deposits represent recent and Quaternary age outwash overlying and cut into the Tertiary Tesuque Formation.

The Tesuque Formation is composed of similar sediments which are more consolidated and cemented. Buried channels of coarse sediment probably occur within the section and influence ground water flow. The Ancha Formation, which unconformably overlies the Tesuque outside the Arroyo, is probably thin or may be absent beneath the valley floor (Spiegel 1963, Fleming 1993). Actual boundaries between these units are not distinguishable in most driller's logs.

Ground water occurs as an unconfined aquifer at depths of 30 to 60 feet in most of this area. Springs and stream bed seeps represent areas where the water table approaches ground level, often associated with geologic contacts or faults.

Local domestic wells are above average for Santa Fe County in terms of production rate, depth to water, and water quality. Domestic wells are partially penetrating, and range from 72 to over 370 feet in the area. The saturated thickness of combined Ancha - Tesuque sediments is greater than 1000 feet, as revealed by exploratory drilling (AGW Consultants, 1976).

### Springs in the Area

Most of the springs and acequias in the area occur along the valley walls of arroyos that drain towards La Cienega, west-southwest of the study area. Based on Spiegel's and Fleming's regional maps, the study area is not in the flow path of groundwater moving towards these springs (Figure 2). In addition, the water table in the study area lies deeper than the discharge elevation of spring lines in Cienega and Guicu Creeks, one to three miles southwest.

Complicating the distribution of the springs is the faulting and degree of stratification in the sediments of the area. For example, at Sunrise Springs, ample groundwater flow (est. 18 gpm) occurs in sand, gravel and clay horizons from depths of 29 to 50 feet, where 15 feet of clay was encountered. The principal water bearing strata was reported as a 5' zone within 16' of "red clay and gravel". The "Sunrise Springs" could be perched flow horizon on the valley wall, where the water table reaches the surface. Spiegel also implicated igneous intrusions or the regional fault to explain these spring locations.

### Aquifer Properties

The sedimentary section appears to be moderately stratified, with interbedded sand and gravel, silt and clay (Appendix 1 and 2). Although moderately transmissive, the aquifer is heterogeneous and anisotropic. In such situations the downstream horizontal hydraulic conductivity is typically much higher than the lateral and vertical hydraulic conductivity (Walton, 1987). A ratio of horizontal to vertical hydraulic conductivity of 10 was used in models presented here.

The average reported hydrologic coefficients of the local formations were reviewed in the Sunrise Springs report. Based on a pump test and other data, that study concluded that an average Transmissivity of 10,000 gpd/ft and a Specific Yield of 0.10 is appropriate and conservative for the combined Ancha - Tesuque formations locally. A Specific Capacity of 1 gal per minute per foot of permeable formation is reasonable in this area. Figure 4 puts these values in perspective.

Using an average water table slope of 0.4 percent, average porosity of 5 percent, and an average hydraulic conductivity of 25 ft/d (31 ft/d was measured in the thin section at Sunrise Springs), the average linear velocity of flow is approximately 1.2 feet per day. Neglecting fracturing, vertical flow velocities are expected to be at least one tenth the rate of horizontal flow.

# Recharge and Contamination Susceptibility

The arroyos flow within their channels seasonally. In this area the stream banks are incised and well defined. Small, seasonal stream flows represent groundwater discharge. Regional ground water through - flow is much larger than vertical recharge due to precipitation, although streambed recharge could be significant during flood events. The arroyos and buried channels are potentially significant conduits of groundwater flow from the mountains (Fleming, 94).

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NOTES: Transmissivity (T)=KM where

K-Permeability
M-Saturated thickness of the aquifer
Specific capacity values based on pumping period of approximately
B-hours but are otherwise generalized.

FIGURE 2-4.—Comparison of transmissivity, specific capacity, and well potential, 163-D-1406.

TAT REGIONAL ESTS 7.5 - 25

	·		. 10-	10,	/FT/MIN	10-1	10-2	10-3	ю-4	R
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	to"	ю*	to <sup>s</sup>	GA Iọ²	_/FTプDAY IO	(gal/fi <sup>2</sup> /day)	10,4	10 E	ю <sup>-5</sup>	ıç
	104	ıç*	10.	METER	S³/METER	Î∕DAY (m/dey 10™		iQ 3	<b>1</b> 0,⁴	10,"
·	VERY KIGH		HIGH	V. REL	TIVE PER	RMEABILITY ATE	LOW	·	VER	T LOW
	Clean gravel		an sand and nd and grave	- F	ENTATIV		<u>LS</u> t, clay and sand, silt			ve cla
	Vesicular and basalt and a limestone an	averno	us	Clean sand and fract igneous a metamor	runed and		i sandstone	•	Massive and metar rocks	

Figure 2-5.—Comparison of permeability and representative aquifer materials, 103-D-1407.

## REPRESENTATIVE VALUES OF AQUIFER MATERIALS

Ta. == ANCHA

Тt TESUQUE

= COMBINED VALUES Tat

Sy = 0.05 - 0.20

Because strata of coarse, unconsolidated sediments underlie the valley, the area has been identified as being susceptible to groundwater contamination, particularly from septic tank effluent. In the 1980 Santa Fe County General Plan, the study area lies in a general outline of areas with potential man - made water pollution problems. However, most of the wells examined for this study report a 3 to 25 feet thick soil and clay near the surface, and many reported 10' to 30' of sandy clay above 60' drill depths. This stratification and the proposed well design should minimize the downward migration of any contaminants.

### FINDINGS

### Prototype Well Design

The objective of the following design is to isolate the Ancha aquifer and produce the underlying Tesuque Formation.

Based on 18 nearby wells the estimated deliverability is 10 to 15 gallons per minute (about half the average driller's estimate). The average well encountered the water table at about 64 feet and was drilled to 144 feet. About 25 feet of well casing was slotted or perforated at various depths. Very little information is reported on pump selection.

Utilizing generalized design considerations as well as conversations with Steve Kuckelman of Kuckelman Pump Services, the following features are estimated (Figure 5). The well should be drilled to 7 7/8" or greater in diameter, approximately 150 to 200 feet deep (i.e. have over a 100 foot water column), utilizing the mud rotary method. Five inch PVC casing should be installed, with more than 25' of slots opposite the most porous and permeable strata at least 50' below the water table.

Presuming the well is capable of pumping at 10 to 20 GPM, a 3/4 to 1 1/2 horse pump rated at 20 gpm, positioned at least 20 feet above total depth, should be sufficient for supplying up to four households.



Grout seal /Bentonite pellets

– Surface casing 💈

Grove feed pipe (tremie)

WT 40'

5" PVC casing

Centering guide

Welded or coupled joint

Well screen /SLOTS

Grovel pack

SAND & GRAVEL

AQUIFER MIL.

Gravel pack tremied to 10-20' above slots Total Screen 25+' in most

TOTAL DEPTH 150-200'

porous & perm. form.

Top of Casing > 1' Above FEMA Floodplain

Surface casing if needed.

Total HEAD 100+'

Bentonite pellets above

gravel pack to surface

3/4 to 1 1/2 hp pump + 20' off bottom

7 7/8+ borehole

SINGLE STRING CONSTRUCTION

Ground surface

FIGURE 11-1.—Gravel packed, rotary drilled well for single string construction. 103-D-1488.

# SUGGESTED PROTOTYPE WELL DESIGN

TO PRODUCE FROM THE TESUQUE FORMATION AND ISOLATE THE ANCHA FORMATION

Prepared by:

Jack P. Frost

Hydrogeologist

505-466-6435

Modified from the Ground Water Manual

A shared well system of this design should be able to serve up to 4 residences restricted to the County's 0.25 acre foot per year allowable. Shared wells will result in about 8 wells per 40 acre tract, versus 16 if each owner is responsible for their own well.

Because of the expected vertical stratification, wells should be perforated in the lowest permeable strata encountered to minimize downward induction of septic effluent. The annulus should be stabilized by gravel pack at least 10 feet above the top of perforations. Above the gravel pack pellet bentonite should be added to near ground level. In this way vertical flow in the borehole annulus will be minimized. This design is similar in some regards to precautions taken in the construction of ground water monitoring wells.

Drilling costs for the proposed design are estimated at \$16 to \$19 per foot (about \$2500 to 3800). The pump and surface equipment was estimated by Mr. Kuckleman at about \$4500 per well.

Mr. Kuckelman estimates that a four - home shared well system could reduce costs as much as 70 percent over single home well systems.

### Well Drawdown Model

For comparison purposes, a well with a pumping rate of 0.60 gallons per minute (864 gpd or 1 acre foot per year), sufficient to serve 4 houses at a 0.25 af/yr allowable, has been modeled in Appendix 3. Actually, such a well typically produces it's average daily output in two to three hours of pumping per day. This translates into an actual, intermittent pumping rate of less than 8 gpm. Intermittent pumping causes a larger transient drawdown with interspersed periods of recovery. Such conditions and results should not be dissimilar to the model scenarios depicted in the Appendix.

The aquifer appears to be more than adequate for domestic use. To test the input assumptions, models were created using both the lower (K=50 gpd/ft, Sy=.05) and higher (K=200gpd/ft, Sy=0.15) estimates of aquifer coefficients. The most conservative drawdown model indicates a maximum drawdown of less than 1 foot in the well bore and less than 0.2 feet at a radius of 100 feet, computed over a 40 year pumping interval.

### Pollution Potential

Because the study area occupies the floodplain and is underlain by porous and permeable sediments, there is some concern for pollution potential. In a conversation with Mr. Gene Fulgenzi, Environmentalist at the District 11 office of the State E.D., he was unaware of any specific problems in the general area.

For the purposes of this study, no information was encountered regarding regional or point source contamination near or up gradient of the study area. Such potential sources include leaking buried tanks, agricultural chemical use or other subsurface disposal hazards.

Septic tanks, the means for domestic liquid waste disposal in this area, create an environment for bacteria to degrade domestic wastes. The effluent from the septic leach field is either transpired by plants or slowly makes its way downward to the water table. In this area the soils and bacterial action should remedial the effluent in a short distance, probably less than tens of feet. The horizontal stratification of the aquifer will also slow the downward percolation of the effluent.

The proposed well construction practices, as well as the natural filter function of the aquifer, should secure bacteria - free groundwater for many years. The State Environment Department specifies construction practices and setbacks from wells, and requires approval of individual septic tank systems.

### SUGGESTED WELL LOCATIONS

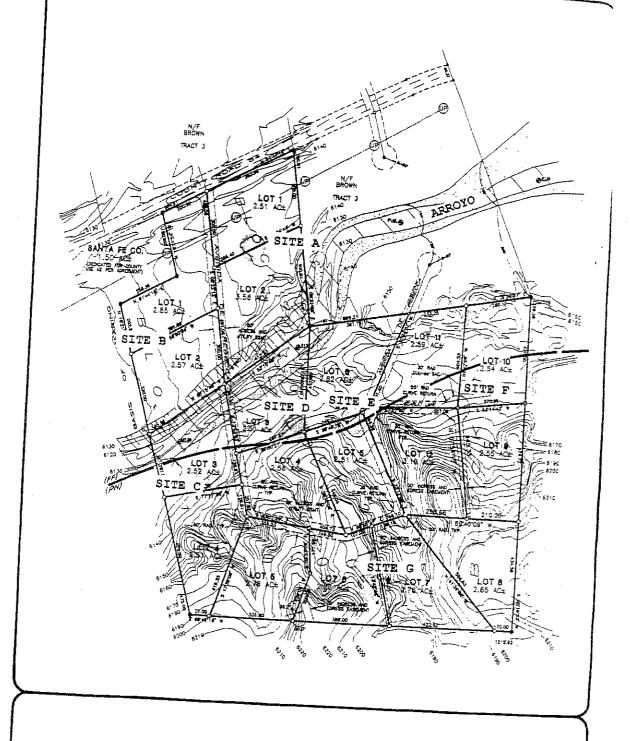
Figure 6 is an orthographic survey plat of the Por Su Gracia Subdivision, showing suggested shared well sites. Approximately 9 sites are recommended, each to be shared by 2 to 3 lots and houses. These locations are based on topography and interpreted homesites. The average distance of water supply line is less than 250 feet. Final homesite choices might cause some adjustments to these suggestions, and some individual wells on the valley walls are likely because of rugged topography.

Considering the well design and model results described previously, well interference should not be an issue in this subdivision.

The following Table indicates lot locations and predicted drilling depths for shared wells located in Figure 6. The proposed depths should access the Tesuque Formation as the principle water bearing formation.

PROPOSED SHARED WELL SITES, ELEVATION, TOTAL DEPTH

Site	Lots Served B=Block, L=Lot#	Estimated Elevation	Estimated Total Depth (ft,app)
А	B2-L1,L2	6142	150+
В	B1-L1, L2	6136	150+
С	B1-L3,L4	6142	150+
D	B1,L3, L4?	6150	200+/-
E	B2-L5, L6	6154	200+/-
F	B1-L9?, L10,L11,L12	6160	200+/-
G	B1-L6,L7	6200	200



SUGGESTED SHARED-WELL LOCATIONS
POR SU GRACIA SUBDIVISION

Prepared by: Jack P. Frost Hydrogeologist 505-466-6435

Page 15

Figure 6

- Computer models depict a modest impact on regional groundwater flow. The cones of depression will not interfere with one another to any significant degree. No impairment of prior ground water appropriators should be expected.
- If State approved practices are employed, the potential for local contamination from domestic septic tank systems appears minimal. The soils and horizontal stratification of the aquifer will remediate and impede downward migrating contaminants.
- A shared well system, coupled with thoughtful well design and construction, will minimize the impact on the aquifer and ensure a safe water supply for the residents of the subdivision.

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Spiegel, Z. And Baldwin, B., 1963, Geology and Water Resources of the Santa Fe Area, New Mexico, USGS Water Supply Paper 1525

Spiegel, Z., 1975, Preliminary Report on the Hydrology of the La Cienega Area, Santa Fe County N.M.: Consultant Report to Santa Fe Downs

Walton, W. C., 1987, Groundwater Pumping Tests, Design and Analysis, Lewis Publishers

### APPENDICES

TABLE OF WELL RECORD INFORMATION

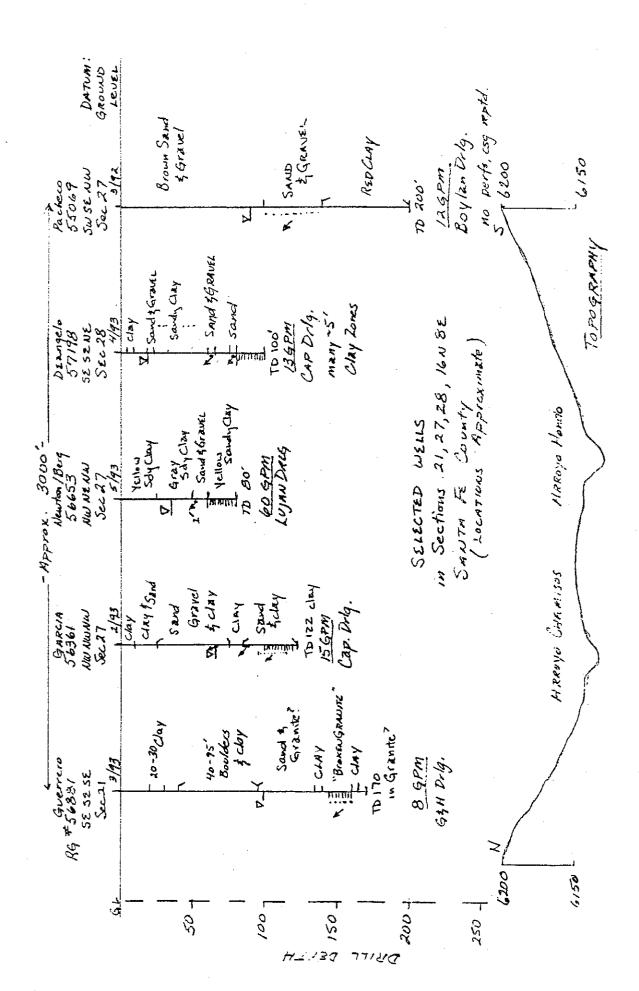
SCHEMATIC WELL LOG CROSS SECTION

PREDICTIVE MODEL USING HIGHER FORMATION COEFFICIENTS

PREDICTIVE MODEL USING MORE CONSERVATIVE COEFFICIENTS

TWO REPRESENTATIVE WELL RECORDS ADJOINING THE STUDY AREA

Well	Owner,	Total	Depth	Yield	Yield Water	Depth to	Principle Water	Perfs.	Drillina
Number	Location	Depth to	to Water	(GPM)	Water (GPM) Column	Base of	Bearing Formation	Casing	Contractor
RG#						Low Zone			
	SE,SE,SE,21	170	100	68	70	160	Pink Bkn Granile	20, 5" pvc	G&H
	SE,SW,SW,22	72	28	NR	44	69	Brown-Red SD	23, 6.625"	Crocker
	NW,NE, NW,27	8	35	60	45	52	Yel. Sand & Gravel	20, 6.625"	Lujan
56361	NW,NW,NW,27	122	92	15	57		Sand & Gravel	20. 5"	Nuanes (Can)
55069	SW,SE,NW,27	200	06	12	110		Sand & Gravel (poor)	40, 7.875" hole	Bovlan
	SE,NE,NE,28	165	4	20	125		Red Grav., Blue Clay & Gravel 30, 4.5" pvc	30, 4.5" pvc	Garcia
57198	SE,SE,NE,28	100	19	13	84		Sand, Sand & Gravel	20	Nuanes (Cap)
58393	58393 SE,SE,NW,22	108	64	20	42	95	Sand & Gravel	20, 5"	Nuanes (Cap)
58245	58245 SE,SE,NW,22	117	69	20	48	44	Sand & Gravel	20, 5"	Nuanes (Cap)
58411	58411 SW,SE,22	105	61	20	4		Gravel	20. 5"	Nuanes (Cap)
55880	55880 SE,NW,SW,27	200	80	50	120	75	Layers of Sand & Gravel	40, 5.5"	Bovlan
55355	55355 NW,NE,SW,27	200	9	10	100		Red & White Clay & Rock	30.4.5"	Garcia
55154	55154 NW,NE,SE,28	96	33	20	57			20.5"	Nilanes
41553	SW,SE,SW,22	100	42	15	58		Gravel	20 6.625"	Rovhal
41775	SE,SE,SW,22	373	125	150	248	370	Brown Sand & Gravel	113. 6.625"	Bovlan
42782	42782 NW,SE,NW,28	90	20	20		80	Gray Silt	20. 6.625"	Boylan
56898	56898 SW,NE,NE,28	160	66	20		53	Sand & Grave	20.5"	Nijanes
56178 F	PERMIT ONLY								000
57760	57760 NE,NE,SE,28	145	75	7		120	"Wash & Boulders	50.4.5"	Thompson
AVERAGES	ES	144.3	63.6	31.2	83.3	111.8			



Program: PT1

Version: IBM/PC 2.1

Model - CIMINATIO

: SIMULATION OF 1 OR 2-LAYER AQUIFER SYSTEM, UNIFORM PROPERTIES, WELL STORAGE CAPACITY, DELAYED GRAVITY YIELD, LEAKAGE, DEWATERING, RADIAL FLOW TO PRODUCTION WELL, FINITE-DIFFERENCE APPROXIMATION FOR PUMPING TEST

DESIGN

Program based in part on program presented by Rushton, K.R. and S.C.Redshaw. 1979. Seepage and groundwater flow-numerical analysis by analog and digital methods. John Wiley & Sons, Ltd. New York; and Rathod, K.S. and Rushton, K.R. 1984. Numerical method of pumping test analysis using microcomputers. GROUND WATER. Vol. 22, No. 5. DATA BASE:

AQUIFER HORIZ. HYDR. COND. (GPD/SQ FT)= 200.00
AQUIFER VERT. HYDR. COND. (GPD/SQ FT)= 20.000
AQUIFER THICKNESS (FT)= 100.00
ARTESIAN AQUIFER STORATIVITY (DIM)= 1.0000D-03
WATER TABLE STORATIVITY (DIM)= 0.1500
PRODUCT. WELL EFFECTIVE RADIUS (FT)= 0.400
TOP OF AQUIFER DEPTH (FT)= 50.00
BASE OF AQUIFER DEPTH (FT)= 150.00
INITIAL WATER LEVEL DEPTH (FT)= 50.00
INFINITE AQUIFER SYSTEM

### COMPUTATION RESULTS:

PRODUCTION WELL DISCHARGE RATE (GPM)= 0.60

PRODUCT. WELL EFFECTIVE RADIUS (FT)= 0.400
TIME AFTER PUMPING STARTED(MIN)=%21024000.00

DISTANCE-DRAWDOWN OR WATER LEVEL VALUES AT END OF PUMPING PERIOD

NODE NO	RADIUS(FT)	DRAWDOWN OR WA	TER LEVEL (FT)
2	0.40	50.08	
3	0.63	50.07	PREDICTIVE MODEL OF DRAWDOWNS
4	1.00	50.07	HIGH K, SY EXAMPLE
5	1.59	50.07	40 YEAR INTERVAL
6	2.52	50.06	
7	4.00	50.06	
8	6.34	50.06	•
9	10.05	50.05	•
10	15.92	50.05	
11	25.24	50.05	
12	40.00	50.04	
13	63.40	50.04	
14	100.48	50.04	
15	159.24	50.03	•
16	252.38	50.03	
17	400.00	50.03	
18	633.96	50.02	
19	1004.75	50.02	,
20	1992.43	50.02	
21	2523,83	50.02	
52	4000.00	50.01	
23	6339.57	50.01	
24	10047.55	50.01	
25	15924.29	50.00	
26	252309_70	50.00	

### DATA BASE:

AQUIFER HORIZ. HYDR. COND. (GPD/SQ FT)= 50.00
AQUIFER VERT. HYDR. COND. (GPD/SQ FT)= 5.000
AQUIFER THICKNESS (FT)= 100.00
ARTESIAN AQUIFER STORATIVITY (DIM)= 1.0000D-03
WATER TABLE STORATIVITY (DIM)= 0.0500
PRODUCT. WELL EFFECTIVE RADIUS (FT)= 0.400
TOP OF AQUIFER DEPTH (FT)= 50.00
BASE OF AQUIFER DEPTH (FT)= 150.00
INITIAL WATER LEVEL DEPTH (FT)= 50.00
INFINITE AQUIFER SYSTEM

### COMPUTATION RESULTS:

PRODUCTION WELL DISCHARGE RATE (GPM)= 0.60

TIME AFTER PUMPING STARTED(MIN)=%21024000.00

DISTANCE-DRAWDOWN OR WATER LEVEL VALUES AT END OF PUMPING PERIO

NO	50.30
	50.30
2 0.40	
3 0.63	50.29
4 1.00	50.27
5 1.59	50.26
6 2.52	50.25
7 4.00	50.23
8 6.34	50.22
9 10.05	50.21 PREDICTIVE MODEL USING LOW-END
10 15.92	50.20 VALUES OF K, Sy
11 25.24	50.18
12 40.00	50.17
13 63.40	50.16
14 100.48	50.15
15 159.24	50.13
16 252.38	50.12
17 400.00	50.11
18 633.96	50.09
19 1004.75	50.08
20 1592.43	50.07
21 2523.83	50.06
22 4000.00	50.04
23 6339.57	50.03
24 10047.55	50.02
25 15924.29	50.01
26 25238.30	50.00

# STATE ENGINEER OFFICE WELL RECORD

### Section 1. GENERAL INFORMATION

') Owner o	of wellDON	NA DEANG	ELO			Own	er's Well No	<u></u>
				as Campa NM			<u> </u>	<del></del>
						-	MEX	
<b>1</b> ,	% <u>SE</u>	SF ME	VE % of S	ection 28	Township.	16N Ra	inge <u>8E</u>	N.M.P.M.
b. Tract	No	of Map No	•	of th	e			
c. Lot h Subd	loivision, recorde	of Block No d in <u>San</u>	ta Fe	of th	e County.			
d. X= _ the _		feet, Y=		feet, N	.M. Coordinate	: System		
						License No	WD 1004	**
Address		Rt 8. Bo	x 331N.	Santa F	e, NM 8	7505		
Drilling Began	4-27-93	Com	pleted <u>4-</u>	27-93	_ Type tools _	Rotary	Size of hol	e <u>7 7/8</u> in.
Elevation of la	nd surface or _			at we	ll is	ft. Total depth	of well	100 ft.
Completed we	llis 🖾 :	shallow 🔲 a	irtesian.		Depth to wate	r upon completion	of well	19 ft.
Denth	in Feet			NCIPAL WATE	R-BEARING S	TRATA		
From	To	Thickness in Feet		Description of	Water-Bearing	Formation	Estimate	ed Yield er minute)
19	22	3	San	d & Grave	<b>21</b>			
60	65	5	San	Sand & Gravel 13 Total				1
75	80	5	San	Sand				
			Section	on 3. RECORD	OF CASING			<del></del>
Diameter (inches)	Pounds per foot	Threads		in Feet	Length	Type of Sho	Per	forations
	per root	per in.	Тор	Bottom	(feet)	Type of She	From	То
5	2.48		0	100	100	NONE	80	100
<del> </del>								
<del></del>			·					
	· .		on 4. RECO	RD OF MUDD	ING AND CEM	IENTING		
Depth From	in Feet To	Hole Diameter	Sac of M		bic Feet Cement	Metho	od of Placement	
	0017					(	93 (	121
	111	l .	1					

То	in Feet	Cotor and type of waterial preconnected 3 7/48
3	3	Sandy Clay
5	2	Sand & Gravel
10	5	Clay
11	1	Sand & Gravel
18	7	Clay
22	3	Sand & Gravel
30	8	Clay & Sand
39	9	Clay
60	21	Sandy Clay
65	5	Sand & Gravel
66	1 '	Clay _
70	4	Sandy Clay
71	1	Sand
75	4	Clay/
80	5	Sand
85	5	Clay
90	5	Sandy Clay
93	3	Sand
94	1	Sandy Clay
99	5	Sand
100	11	Clay
	3 5 10 11 18 22 30 39 60 65 66 70 71 75 80 85 90 93 94	3 3 5 2 10 5 11 1 18 7 22 3 30 8 39 9 60 21 65 5 66 1 70 4 71 1 75 4 80 5 85 5 90 5 90 5 93 3 94 1 99 5

Section 7. REMARKS AND ADDITIONAL INFORMATION

# STATE ENGINEER OFFICE WELL RECORD

		Se	ction 1. GEN	ERAL INFO	RMATION			
		87_ 3 ±=	D Mouton	/ Terry	Bera	Owner's We	ll No	
wner of well		He len	POR 200	)		<u>- 193 JHN</u>	7 00 10	
treet or Post	Office Address	Canta	Fe, NM B	7501			<u>, da 48</u>	<del>26</del>
ter and Chuta		Santa	re, m, o	7.3.2	d is located in th	VILLE FA	'Olumba 👡	_
as drilled und	er Permit No	10 300		27 7	ownship <u>16</u> N	<b>-</b>	U 11 - 21 11 - vo	<b>Ф.М.Р.М.</b>
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. Tract No	o	f Map No		of the				
	£5	lock No		of the				_
c. Lot No	OIE	Sant	a Fe	Cour	ity.			
Subdivisio	n, recorded m				a di cas Cont			_Zone in
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a. x							_	
		Tud-	n Drillin	na .	I	icense No. WD-5	47	
Drilling Cont	tractor	OR WILLIAM STREET						
		₽₩	3. Box 9	5-78, Sant	a Fe, NM 8	7.505		
ess		Rt.				1	nes at hala	9 in.
29	= 1 <b>/-</b> 02	Commis	ted 5-14-	93	Type tools $ \frac{R}{R}$	otary	_ Size of note	1181
ng Began	J-14-23	Comple				ft. Total depth of	wali	80 ft.
- 1%				at well i	s	ft. Total depun of	w C11	
tion of land	surface of					pon completion of	well	<u>35                                    </u>
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		<del></del>			DEADING CTD	ATA		
		Section	on 2. PRINCI	PAL WATER	BEARING STR	1	Estimated	Yield
Depth in	Feet	Thickness	The	ecription of W	ater-Bearing For	mation	(gallons per r	ninute)
	To	in Feet	De	arriberan ar				. 7
From			Yellow Sand & Gravel 60 o					
50	52	2 Yellow Sand & Graver						
	_							
		<u> </u>						
1								
						Ì		
1								
			0, 141.	3. RECORD	OF CASING			
					1 1		Perf	orations
Diameter	Pounds	Threads	Depth		Length (feet)	Type of Sho	From	To
(inches)	per foot	per in.	Тор	Bottom				00
			0	80	1		60	80
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		Sect	tion 4. RECO	RD OF MUD	DING AND CEM	IENTING		<u>.                                    </u>
Denth	in Feet	X Hole	Sac	ks	Cubic Feet	Meth	od of placemen	t
Lom	To	Diameter	of M	lud	of Cement			
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		Y :					R 0F	

_	То	in Feet	Color and Type of Material Encountered 56653
0	25	25	Yellow - Sandy Clay
25	50	25	Gray - Sandy Clay
50	60	10	Yellow Sand & Gravel
60	80	20	Yellow - Sandy Clay p 5
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Section 7. REMARKS AND ADDITIONAL INFORMATION

# **JACK PHILIP FROST**

GEOLOGIST, HYDROLOGIST (505) 466-6435

RT. 3 BOX 95-37 SANTA FE, NM 87505

### Transmittal Letter

To: Mr. Charles Heaton
Mr. Joe Catanach
Santa Fe County Land Use

September 28, 1994

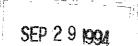
### Re: Vista de Sandia Subdivision

Enclosed is an addendum to the hydrogeologic study I prepared for the aforementioned subdivision. Please include this in the submittal package for the project. I find sufficient water availability to support 2.5 acre development in the area.

Would you please review the attached addendum and call me if you have any questions? My investigations in this area are ongoing, and I will promptly notify you of any new or revised findings. Feel free to call me if I can be of any assistance.

Sincerely,

Jack P. Frost



### ADDENDUM TO HYDROGEOLOGIC REPORT

Re: Por Su Gracia , Vallecitas de Gracia, and Vista de Sandia Subdivisions

Calculations of Water Availability beneath 2.5 acre tracts in Subject Area.

Prepared by Jack P. Frost, Hydrogeologist

This memo supplements the hydrologic studies I have prepared in sections 21, 22, 27, and 28, T16N, R8E, Santa Fe County. As mentioned in the reports, there are a number of pumping tests in the area, to the east at the Racetrack, to the southeast at La Canada Subdivision, and to the west at Sunrise Springs. The findings of hydraulic coefficients from these tests are characteristic of the Ancha and Tesuque formation aquifers. Sample and geophysical logs for a uranium test hole beneath the subject area are attached, demonstrating the presence of a thick section of saturated Tesuque aquifer. I believe the Ancha-Tesuque contact occurs at about 70 feet in this well. Permeable Tesuque sands occur at 120', 160, and 200' which are suitable for a domestic well completion.

A calculation of the County Code-prescribed Water Availability follows. This calculation is based on the generalized well design proposed, having total depth of 200 feet and a Saturated Thickness of 135'. A 100 year availability of 0.1134 acre foot per acre per year is calculated. This results in an availability beneath a 2.5 acre tract of 0.2835 acre feet per year. The County permits 2.5 acre densities with a restriction on water use of 0.25 acre feet per year in this area. Again, the wells in this area could be drilled deeper to demonstrate greater availability, but this would be unnecessary. The average depth of 18 domestic wells in the immediate vicinity is 144 feet.

Also attached is a revised computer flow model demonstrating the predicted drawdowns pumping 1 acre foot per year for 100 years (allowable for 4 lots sharing the well). Conservative coefficients were used in this calculation, and it demonstrates a modest drawdown of less than 2 feet at radii greater than 160' from the modeled well. According to this model well interference will be negligible. This model does not consider the presence of many hundreds of feet of Tesuque formation not penetrated in the proposed well design.

If you have any questions about these findings please call me at 466-6435.

# WATER AVAILABILITY PER CODE PRESCRIBED CALCULATION VICINITY OF SECTIONS 21, 22, 27 and 28, T16N, R8E

Prepared by Jack P. Frost

note: In this area the prevailing County Code permits single dwelling lots to 2.5 acres when restricted to a 0.25 acre foot per acre per year water use.

### STORAGE CALCULATION

Storage, per acre = Sy x ST x Rl x Rec

**Sy** = 0.15 Standard Value

ST = 135' of Tesuque formation

Rl = 0.7 per Code

Rec = 0.8 per code

 $S' = 0.15 \times 135' \times 0.7 \times 0.8 = 11.34 \text{ acre feet per acre}$ 

note: ST derived from a depth to water of 65' (average in nearby water wells) and TD of 200'. All wells in this area are partially penetrating. The Saturated Thickness of Tesuque formation exceeds 800'. Several wells at Santa Fe Downs and elsewhere produce from commingled Ancha-Tesuque formations to depths of 740 feet.

### WATER AVAILABILITY

Per the Code calculation, water availability beneath the subject tract presumes storage depletion and requires the water supply to last 100 years. However, the average published service life of domestic water wells (neglecting pumps) is 35 years.

A, PER ACRE = 11.34 ACFT/AC % 100 YEARS = 0.1134 ACFT/YR

AVAILABILITY PER 2.5 ACRE TRACTS = 0.2835 ACFT/YR

ogram: PT1

rsion: IBM/PC 2.1

: SIMULATION OF 1 OR 2-LAYER AQUIFER SYSTEM,

UNIFORM PROPERTIES, WELL STORAGE CAPACITY, DELAYED GRAVITY YIELD, LEAKAGE, DEWATERING,

RADIAL FLOW TO PRODUCTION WELL, FINITE-

DIFFERENCE APPROXIMATION FOR PUMPING TEST

DESIGN

rogram based in part on program presented , Rushton, K.R. and S.C. Redshaw. 1979. Seepage nd groundwater flow-numerical analysis by nalog and digital methods. John Wiley & Sons, Ltd. w York; and Rathod, K.S and Rushton, K.R. 1984. imerical method of pumping test analysis using icrocomputers.GROUND WATER.Vol.22,No.5.

ress any key to continue

GROUNDWATER FLOW MODEL LA CIENEGA VICINITY TESUQUE FORM. COEFFICIENTS Unconfined Aquifer Th = 100', Kh = 5 gpd/ft2Kh/Kv = 10

Prep. By JPF,9/94

### ATA BASE:

QUIFER HORIZ. HYDR. COND. (GPD/SQ FT)= 5.00 QUIFER VERT. HYDR. COND. (GPD/SQ FT)= 0.500 QUIFER THICKNESS (FT) = 100.00 RTESIAN AQUIFER STORATIVITY (DIM)= 1.0000D-03 ATER TABLE STORATIVITY (DIM)= 0.1000 RODUCT. WELL EFFECTIVE RADIUS (FT)= 0.400 OP OF AQUIFER DEPTH (FT)= 50.00 BASE OF AQUIFER DEPTH (FT)= 100.00 NITIAL WATER LEVEL DEPTH (FT)= INFINITE AQUIFER SYSTEM

# COMPUTATION RESULTS:

lacftlyr. PRODUCTION WELL DISCHARGE RATE (GPM)= 0.62

FIME-DRAWDOWN OR WATER LEVEL VALUES (FT)

## SELECTED DISTANCES (FT)

TIME (MIN)	0.40	63.40	159.24	400.00	1004.75	2523.83
0.14 0.23 0.36 0.57 0.91 1.44 2.28 3.62 5.73	50.02 50.04 50.06 50.09 50.14 50.22 50.33 50.49 50.71	50.00 50.00 50.00 50.00 50.00 50.00 50.00 50.00	50.00 50.00 50.00 50.00 50.00 50.00 50.00 50.00	50.00 50.00 50.00 50.00 50.00 50.00 50.00 50.00	50.00 50.00 50.00 50.00 50.00 50.00 50.00 50.00	50.00 50.00 50.00 50.00 50.00 50.00 50.00 50.00 50.00

Service Servic						
14.40	51.35	50.00	50.00	50.0 <b>0</b>	50.00	50.00
22.82	51.74	50.01	50.00	50.0 <b>0</b>	50.00	50.00
36.17	52.12	50.03	50.00	50.00	50.00	50.00
57.33	52.47	50.06	50.00	50.00	50.00	50.00
90.86	52.75	50.12	50.00	50.00	50.00	50.00
144.00	52.98	50.20	50.01	50.00	50.00	50.00
228.22	53.17	50.30	50.04	50.00	50.00	50.00
361.71	53.33	50.41	50.07	50.00	50.00	50.00
573.27	53.47	50.51	50.13	50.00	50.00	50.00
908.58	53.60	50.62	50 <b>.19</b>	50.01	50.00	50.00
1440.00	53.72	50.72	50.26	50.02	50.00	50.00
2282.25	53.82	50.81	50.34	50.04	50.00	50.00
3617.12	53. <del>9</del> 1	50. <del>9</del> 0	50.41	50.07	50.00	50.00
5732.74	54.00	50.97	50.47	50.10	50.00	50.00
9085.79	54.07	51.04	50.53	50.13	50.00	50.00
14400.00	54.13	51.10	50.58	50.16	50.01	50.00
22822.47	54.19	51.15	50.63	50.19	50.01	50.00
36171.17 ·	54.24	51.19	50.67	50.22	50.01	50.00
57327.44	54.28	51.24	50.72	50.25	50.02	50.00
90857.87	54.33	91.10	50.75	50.28	50.02	50.00
144000.03	54.37	51.32	50 <b>.79</b>	50.32	50.03	50.00
228224.66	54.42	51.36	50.83	50.35	50.04	50.00
361711.72	54.47	51.41	50.88	50.39	50.06	50.00
573274.44	54.52	51.46	50.93	50.43	50.08	50.00
908578.77	54.60	51.53	51.00	50.49	50.11	50.00
%1440000.31	54.68	51.61	51.08	50.56	50.15	50.00
%2282246.70	54.78	51.70	51.17	50.65	50.21	50.01
<b>%3617117.27</b>	54.90	51.81	51.27	50.75	50.28	50.03
<b>%5732744.56</b>	55.02	51.92	51.38	50.86	50.37	50.05
<b>%9085787.88</b>	55.15	52.05	<b>51.50</b> ,		50.47	50.10
%14400003.42	55.2 <b>8</b>	52.17	51.63	51.09	50.58	50.16
%22822467.51	55.42	52.30	51.76	51.22	50.70	50.25
<b>%36171173.56</b>	55.57	52.44	51.89	51.35	50.82	50.34
<b>%52560000.00</b>	55.69	52.55	52.00	51.46	50.93	50.43

TIME AFTER PUMPING STARTED(MIN)=\$52560000.00 = 1004 rs

### DISTANCE-DRAWDOWN OR WATER LEVEL VALUES AT END OF PUMPING PERIOD

NODE NO	RADIUS(FT)	DRAWDOWN OR WATER LEVEL (FT)
2	0.40	55.69
3	0.63	55.39
4	1.00	55.10
5	1.59	54.81
6	2.52	54.52
7	4.00	54.23
8	6.34	53.95
9	10.05	53.66
10	15.92	53.38
11	25.24	53.10
12	40.00	52.82
13	63.40	52.55
14	100.48	52.27
15	159.24	52.00
16	252.38	51.73
17	400.00	51.46
18	633.96	51.19
19	1004.75	50.93
20	1592.43	50.67
21	2523.83	50.43
22	4000.00	50.23
23	6339.57	50.08
24	_ , , , , , ,	50.02
25	15924.29	50.00

### DRILL HOLE RECORD

INSTRUCTIONS: This form should be executed in duplicate, preferably typewritten, and submitted to the near est district office of the State Engineer. All sections pertaining to the specific drill hole shall be any as completely, and accurately as possible. Any additional remarks or information pertainent to the plug construction and operation and maintenance of the drill hole should be included in Section 7.

Section 1 (A) Owner of land or lessee\_ Street and Number City South Fo 137 Hole is located in the NE 1/4 NE Rge. (B) Drilling Contractor. Street and Number 1 Caspec Drilling: Commenced Seb // 197/Completed (Plat of 640 acres) Elevation at top of casing in feet above sea level \_\_\_ .Total depth of hole \_ Check whether water encountered is Shallow or arresian. Depth to water upon completion 23 Section 2 PRINCIPAL WATER-BEARING STRATA Depth in Feet Thickness in No. Description of Water-Bearing Formation From Feet 1 840 Interbedded Sand Stone + Mudchase 2 3 4 Section 3 RECORD OF CASING Dia Pounds Depth Threads Perforations Type Shoe. in. ft. Top Bottom From Tα Section 4 RECORD OF MUDDING AND CEMENTING Depth in Feet Diameter Tons No. Sacks of From Hole in in. Methods Used To Clay Cement PLUGGING RECORD Company Personel Name of Plugging Contractor\_\_\_ Street and Number. State Tons of Clay used Tons of Roughage used. Type of roughage Plugging method used Pluglic hale plug @ 30' Y Filled Date Plugged 3/10 Plugging approved by: Cement Plugs were placed as follows: Depth of Plug Basin Supervisor No. of Sacks Used From FOR USE OF STATE ENGINEER ONLY 30 Date Received

Use

16.8.28.222

Location No. \_

File No.

	<del></del>	<del>,</del>		7. HOLE
From	in Feet	Thickness in Feet	Color	Type of Material Encountered
0	+	<del> </del>		
153	135	155-	<u> </u>	S.S. + Gravel ups Mudebone Muck love uif Sandsbone Sandy Mudebone
305°	305	150 95	Aca .	Much hover Ulf Sandsbore
	400		Ben-gry	Sandy Mudshire
400	465	45	_Ben-gin	Mudetnee
465	630	165	Bea	Muddy SS,
430	680	50	Ben	M.S.
680	725	25	Bra	Mudde SS
<u> 725 - </u>	840	6.5	н	Mudistare
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3 - MI - 1 J AME - 10				
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Section 7. Remarks and additional information

The undersigned hereby certifies that, to the best of his knowledge and belief, the foregoing is a true and correct record of the above described hole.

/**3/** 

HULE NU. \_\_\_\_\_/ 87 EAST. 1160 LOGGE BY Morris-Groupate 2/13/71 22 TOWNSHIP 16 N 8E 840' RANGE \_\_\_ NE NE NE GEOPHYSICAL LOG DEPTHPCA LITHOLOGY LOG Alluvium brn SS + gv) Ancha channe brn sdy mdst brn SS, m-c brn sdy clyst (250005 100 orn mody 55 brn sdy clyst brn interb SS + mdst brn mast. 200hrn-dk brn mdst, sm lt grn cly (abd @ 250:) dk brn mdst grnish-gry clyst + brn mdst olive-gry clyst blue-gry clyst brn mdst + gry clyst 300 brn mdat 20.  $\overline{+}$ brn mdst, with wh clyst It grn + wh clyst, with brn mdst brn mdst brn mdst, sm grn clyst 4∞ -∃ grnish-gry clyst brn mdst grn mdst brn with sm grn mdst 132 brn mdst, abd dk grn mdst

HOLE SIZE THE LE AIR LE MATER HULE NU. ----160' LOSED EMORTIS-Green DATE 2/18/71 <u>38</u> TOWNSHIP 16 N RANGE RE 8'40' DEPTHPCA GEOPHYSICAL LOG LITHOLOGY LOG brn sdy mdst brn mddy 55 600 brn sdy mdst brn mddy SS 700brn sdy mdst 20111111 1 836' TD Other tests to 1000' this area. In 900 /33



Top of Casing > 1'
Above FEMA Floodplain

Surface casing if needed.

Total HEAD 100+'

Bentonite pellets above gravel pack to surface

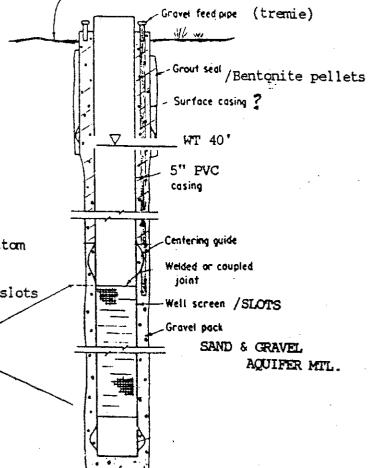
3/4 to 1 1/2 hp pump + 20' off bottom

Gravel pack tremied to 10-20' above slots

Total Screen 25+' in most porous & perm. form.

TOTAL DEPTH 150-200'

7 7/8+ borehole



SINGLE STRING CONSTRUCTION

Ground surface

FIGURE 11-1.—Gravel packed, rotary drilled well for single string construction. 103-D-1488.

# SUGGESTED PROTOTYPE WELL DESIGN

TO PRODUCE FROM THE TESUQUE FORMATION
AND ISOLATE THE ANCHA FORMATION

Prepared by: Jack P. Frost

Hydrogeologist

505-466-6435

Modified from the Ground Water Manual

/34

age 11

### DECLARATION OF COVENANTS, CONDITIONS, AND RESTRICTIONS

This Declaration of Covenants, Conditions and Restrictions is made on this 29 day of February 1996, be VISTA DE SANDIA CORPORATION hereinafter called "Declarant".

WHEREAS, Declarant is the owner of the real property located in Sections 21 & and 22, Township 16 North, Range 8 East, N.M.P.M., County of Santa Fe, New Mexico and commonly known as the Vista De Sandia Corporation Subdivision and recorded in the office of the County Clerk, Santa Fe, New Mexico, Plat Book 333 Page 45, hereinafter called "the Property": and

WHEREAS, Declarant wishes to impose the provisions of this declaration on the subject Property to the Covenants, Conditions and Restrictions stated in this document, including easements, for the purpose of protecting the value and standards of said property, and to insure that all owners will maintain the Property in a private and prestigious manner; and

WHEREAS, the terms of this declaration shall run with the land and be binding upon and inure to the benefit of all parties having any right, title or interest in or to the Property, or any part thereof, and their successors and assigns,

IT IS, THEREFORE, DECLARED:

### **ARTICLE 1 - DEFINITIONS**

- 1. "OWNER" shall mean and refer to any contract purchaser of record owners, whether one or more persons or entities, of a fee simple title to any lot which is a part of the Property, but excluding those having such interest merely as security for the performance of an obligation.
- 2. "Property" shall mean the above described real estate.
- 3. "Lot" shall mean and refer to any plot of land shown within the Property whether existing now, or by virtue of any subsequent division of the Property.
- 4. "Declarant" shall mean and refer to Vista De Sandia Corporation Subdivision.

### ARTICLE II - USE OF PROPERTY; STRUCTURES

- 1. The Property or lots shall be used for residential purposes.
- 2. It is expressly stated that any space within a residence located on any lot on the Property may be used for a professional or other office in which there is employed not more than two (2) employees or other persons who do not reside on the Property or the Lot, provided that said use of the Property does not generate a greater level of traffic or activity on the Lot than would normally be generated by a single family dwelling.



- 3. No structure shall be erected, altered, placed or permitted to remain on any Lot or building other than one single-family dwelling.
- 4. No building shall be erected any closer than twenty-five (25) feet to any boundary line of any lot within the Property.
- 5. Exterior construction of any type on any Lot shall be completed within eighteen (18) month of commencement of said construction.
- 6. All barns, stables or corrals for confining horses or animals permitted under this declaration shall not occupy more than six percent (6%) of the total land area of any lot. Such structures shall be of good and sound design and construction.

### ARTICLE III - PROHIBITIONS

- 1. No division of any lot shall be permitted.
- 2. Vehicles in need of repair, wrecked vehicles, vehicles that are not in operating condition will not be allowed on any lot in this subdivision whatsoever. Modular, manufactured housing or double wide mobile homes (not older than 1990) will be allowed on any lot within the Property.
- 3. No animals shall be raised or maintained on any lot for commercial use. No commercial breeding will be allowed. No owner shall be allowed to maintain a number of animals on any lot which could cause a health or environmental hazard to other lot owners on the Property.
- 4. No oil drilling, oil development operations, oil refining, quarrying or mining operations of any kind shall be permitted on any lot on the Property. No oil wells, tanks, tunnels, mineral excavations or mine shafts shall be permitted on the Property. No derrick or other structure designed for use in boring for oil, natural gas, or any other substance, with the exception of water for domestic use, shall be erected, maintained or permitted on any lot.
- 5. No dumping of solid or liquid waste shall be permitted on any lot.
- 6. No hunting shall be permitted on the Property and no discharge of firearms shall be permitted on the Property.
- 7. No storage of building materials other than during construction shall be permitted. No storage of any materials except those commonly and regularly used in connection with a residence shall be permitted. No storage of any explosives or hazardous materials of any kind shall be permitted.
- 8. Bright, glaring lights on rooftops, poles, patio walls or elsewhere are prohibited. All exterior lights must be located so as not be directed toward surrounding lots, properties or roads.
- 9. No lot shall be used for the storage or dumping of trash, rubbish, debris or waste of any kind, or for the storage of any Property or thing which causes such lot to appear in unclean or untidy condition, or that will be visually offensive or obnoxious, and no substance, thing or material may be kept upon any lot which will emit foul or obnoxious odors, or that will cause any noise that will disturb the peace, quiet, comfort or serenity of any occupant or owner of any lot within the Property.
- 10. No guest houses shall be allowed on any lot.